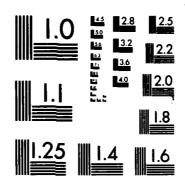
LIGHTWEIGHT TOWED HOWITZER DEMONSTRATOR PHASE 1 AND PARTIAL PHASE 2 VOLUM (U) FMC CORP MINNEAPOLIS MINN NORTHERN ORDNANCE DIV R RATHE ET AL APR 87 FMC-E-3041-VOL-E DAAA21-86-C-0047 F/G 19/6 AD-A183 995 1/2 UNCLASSIFIED NL



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Lightweight Towed Howitzer Demonstrator

Final Report

Volume E

Hydraulic Component Design by York

April 1987



Contract Number DAAA21-86-C-0047

Approved for public released betimilar notification betimilard

FMC Corporation Northern Ordnance Division 4800 East River Road Minneapolis, Minnesota 55421

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SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered)

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The LTHD (Lightweight Towed Howitzer Demonstrator) was to be a 9,000 lb equivalent to the M198, transportable via Blackhawk helicopter, with reduced emplacement time using fewer personnel. The FMC design achieved weight reduction via a mortar-like configuration, composites structure, and hydraulic actuators. Recovery of power from the recoil system, in turn, facilitated crew reduction via hydraulic emplacement, four-way joystick tube lay, and power ramming. FMC completed Concept Development (Ph I) and two-thirds of Detailed Design (Ph II) prior to funds running out.

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number)

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Vol/Sec	Description
E	Hydraulic Component Analysis by York
E/050	Table of Contents
E/100	Final Status Report
E/110	Accumulator Unit Assembly Part Number T-12585720
E/111	Accumulator Unit Assembly (obsolete design)
E/120	Equilibration Accumulator 5720-003 See E/510 for Accumulator Vol Indicator Assy
E/121	Equilibration Accumulator (obsolete design)
E/130	Reservoir Accumulator
E/131	Reservoir Accumulator (obsolete design)
E/140	Breech Actuator 5725
E/141	Breech Actuator (obsolete design)
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E/151	Counterrecoil Accumulator - left (obsolete design)
E/160	Counterrecoil Accumulator - right 5718
E/170	Elevation Actuator 5716
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E/191	Equilibration Actuator - left (obsolete design)
E /200	Equilibration Actuator - right 5712
E/210	Lanyard Actuator 5727
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E/220	Latch Position Actuator 5728
E/221	Latch Position Actuator (obsolete design)
E /230	Primer Actuator 5726
E/231	Primer Actuator (obsolete design)
E/240	Rammer Actuator
E/241	Rammer Actuator (obsolete design)
E/250	Traverse Actuator
	See E/500 for Bear-Loc Intensifier Assy DTHC TAB
E/251	Traverse Actuator (obsolete design) Ulannomiced
E/260	Walking Beam Actuator - LH front 5721 Justification
E/251	Walking Beam Actuator - LH front (obsolete design)
B /270	Walking Beam Actuator - LH rear 5722
E/280	Walking Beam Actuator - RH front 5723
B /290	Walking Beam Actuator - RH rear 5724 Distribution
E/500	Bear-Loc Intensifier Assy
B/510	Accumulator Vol (piston position) Indicator Assy
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DESCRIPTION: FINAL STATUS REPORT

STATUS - PER FMC:

The hydraulic component designs are well integrated with system design. The performance requirements appear feasible. The total weight budget (established by early FMC estimates) appears realistic.

Some preliminary discussions with metallurgists familiar with titanium suggest it may be feasible as a hydraulic cylinder and rod material which could, in turn, facilitate a further weight reduction. Other discussions regarding AlSiCp also suggested this material suitable as a hydraulic cylinder material. Neither approach was pursued, but both suggest additional weight reduction is feasible.

The only known problem remaining is potential overloading of the walking beam actuators due to road input (see E/260, E/270, and C/270).

The component paragraphs within this section are repeated within the component sections for clarity.

AUTHOR: Jeff Ireland/Bart Anderson

FINAL REPORT

PMC LIGHTWEIGHT TOWED HOWITZER DEMONSTRATOR Hydraulic Components

P. O. P68622-84-LMHD

York Industries, Inc. 1750 Toronita Street York, PA 17402 Phone: 717-846-1988 (81616)

Final Status Report FMC Hydraulic Component Design P.O. P68622-84-LWHD

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Final Status Report FMC Hydraulic Component Design P.O. P68622-84-LWHD

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1.0 Introduction and Summary

This is the final status summary report for the design of the LWTHD hydraulic components assigned to York Industries Inc. as of March 13, 1987. The design effort had reached the final stage with part detailing begun. The design concept phase had been completed on all components except the Walking Beam Actuators. Per FMC direction, one 9 track magnetic tape copy of the CAD drawing files and a set of B-size reproducible drawings is enclosed. Table 1 lists those drawings which are being submitted. A comparison of estimated weight to the allotted weight budget is presented by Table 2. The performance analysis of the elevation subsystem was begun, but suspended early in the program.

2.0 Overview:

The Aerospace Division of York Industries Incorporated (YII) was under contract to FMC, Northern Ordinance Division, to provide a number of hydraulic components for the Lightweight Towed Howitzer Demonstrator (LETHD) program. This effort consisted of the design of each component, an analysis of the performance and structural adequacy and the delivery of an assembly drawing at the completion of program Phase 2. Fabrication and delivery of hardware was anticipated in a later Phase 3 follow-on.

State-of-the-art technology was to be employed in this effort. The equilibration and traverse actuators employed the YII patented BearLoc position locking actuator for obtaining and holding azimuth and elevation aiming. Kevlar wrapping of actuators and accumulators was used to minimize weight and to provide resistance to fragmentation, both of which had been qualified on earlier programs. The materials of construction, corrosion protection and thin wall cylinder fabrication techniques had all been demonstrated on prior programs, therefore, the bulk of the technology demonstration effort in the LWTHD program could be directed to the non-hydraulic aspects.

3.0 Component Design Status:

The design status for each component is described below. Those components whose part numbers are grouped utilize a single design with only minor mounting differences. The design effort consists of the following sub-phases which were used for internal YII tracking of progress against cost, schedule and weight budgets. The "Concept design" sub-phase defines the basic configuration of the component and matches it to the required space and performance envelope. The "Initial Assembly" sub-phase refines the concept drawing by adding the load attachments and ports, and by conducting the first analysis directed at reducing weight. The "Final Assembly" sub-phase consists of assigning part numbers to the detail parts, conducting a detail level stress analysis of critical regions and an independent evaluation of piece part fabricability. The "Detailing" sub-phase generates drawings for each of the piece parts contained in the component assembly.

P/N T-1257 5712/B - ACTUATOR, EQUILIBRATION - RIGHT SIDE P/N T-1257 5713/B - ACTUATOR, EQUILIBRATION - LEFT SIDE

The assembly drawing was nearing completion and the stress analysis was begun. This component had been identified by YII as a long lead item and the design was scheduled for fabrication process review and assembly tooling design. This component was well within its weight budget after Kevlar wrapping of the actuator cylinder was incorporated.

P/N T-1257 5714/B - ACTUATOR, TRAVERSE

The concept drawing is complete but the the stroke must be changed to the requirements of the March 6 coordination meeting. The projected weight estimate is over the allotted target weight due to the increase in stroke, thus another weight reduction pass would have been required.

P/N T-1257 5716/C - ACTUATOR, ELEVATION
P/N T-1257 5717/A - ACTUATOR, ELEVATION - LEFT SIDE (deleted)

A single actuator, attached to the center of the slide, was substituted for the original one on each side and the stroke was lengthened. The concept drawing for the revised stroke was completed and was in review for fabrication evaluation. The projected weight of this actuator meets its weight budget, however, further reduction was planned to allow for the weight growth in the Counter-recoil Accumulators as discussed later. Tailoring of cushioning at end of stroke is planned whenever the acceleration requirements become defined.

P/N T-1257 5718/B - ACCUMULATOR, COUNTER-RECOIL - RIGHT SIDE P/N T-1257 5719/B - ACCUMULATOR, COUNTER-RECOIL - LEFT SIDE

The concept drawing for these accumulators is approximately 90 % complete, however, the increase in volume from 1600 cubic inches to 2400 inches drives its estimated weight above the target weight by a significant amount. In the interest of weight reduction, it is recommended that the factor of safety on maximum operating pressure for proof pressure be reduced from the standard value of 2.0 to a value of 1.5 and that the burst factor be reduced from 4.1 to 3.0 on the cylindrical section only. Design factors of safety for the end caps and threaded joints remain at the standard level of 4.0. FMC approval was obtained at the March 6, 1987 coordination meeting.

P/N T-1257 5720/B - ACCUMULATOR UNIT, FEED & EQUILIBRATION

The newly defined port manifold was being added to the concept drawing of the Accumulator Unit at the time of contract termination. The mounting techniques for both accumulators had been defined and coordinated with FMC. The front slide mount carries both axial and radial loads. Slip joints are used at the mid-slide mount so that expansion of the accumulators does not load the slide, therefore only radial loads are carried. The piston position indicators are located near the mid-slide mount. The YII request for an evaluation of readability of position indicators as shown by the concept drawing was still pending.

P/N T-1257 5720-1/B - ACCUMULATOR, EQUILIBRATION
P/N T-1257 5720-2/A - ACCUMULATOR, EQUILIBRATION (deleted)

The concept drawing of the equilibration accumulator had been completed and the assembly drawing was being revised to change the length of the accumulator to facilitate its mounting to the slide. This component meets its weight budget and was in fabricability review. The length of the cylinder of this accumulator was set by the need to match the length of the Feed Accumulator as a means to minimize overall system weight, however, this length forced this component into the list of long lead items being prepared at the time of contract termination.

P/N T-1257 5720-3/B - ACCUMULATOR, FEED

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The concept drawing for the feed accumulator is complete and the assembly drawing was being revised to change the length of the accumulator to facilitate its mounting to the slide. This component meets its weight budget and was in fabricability review. The length of the cylinder of this accumulator was set by the need to match the length of the Equilibration Accumulator as a means to minimize overall system weight.

P/N T-1257 5721/B - ACTUATOR, WALKING BEAM - LH FRONT P/N T-1257 5723/B - ACTUATOR, WALKING BEAM - RH FRONT

The concept drawing on this component had been completed and the assembly drawing was being revised to incorporate 2 inches of free travel in the transit mode. Several approaches to obtain free travel were being evaluated which would have been added to the assembly drawing when complete. The design provisions for free travel were being evaluated on the rear actuators and would have been added to these actuators when complete. An extended stroke pin lock was incorporated into the actuator. This lock is actuated by hydraulic pressure and provides a flag of lock/unlock status. The assembly drawing was being revised to mount the FMC specified control valve directly on the actuator. This unit, as revised, exceeds its weight budget by 20% and required further design effort directed at weight reduction.

P/N T-1257 5722/B - ACTUATOR, WALKING BEAM - LH REAR P/N T-1257 5724/B - ACTUATOR, WALKING BEAM - RH REAR

The concept drawing on this component had been completed and the assembly drawing was being revised to incorporate 2 inches of free travel in the transit mode. Several approaches to obtain free travel were being evaluated which would have been added to the assembly drawing when complete. The extended stroke pin lock was also incorporated into the actuator. The assembly drawing was being revised to mount the FMC specified control valve directly on the actuator. This unit, as revised, exceeds its weight budget by 20% and required further design effort directed at weight reduction.

P/N T-1257 5725/A - ACTUATOR, BREECH

The concept drawing for the Breech actuator had been completed and the assembly drawing was being revised to incorporate a check valve and FMC specified port locations. The pilot operated check valve provides an extended stroke position lock when hydraulic pressure is removed from the unit. This unit meets its weight budget and no further weight reduction is required.

P/N T-1257 5726/A - ACTUATOR, AUTO-PRIMER

The concept drawing on this actuator was approximately 80% complete. Design provisions for extensive flexing of its mount and adjacent components were being evaluated. The weight of this unit exceeds its budget due to the extensive manifold incorporated into its requirements. Since, there is little expectation of being able to reduce its weight to the budget level, it was recommended that its weight budget be appropriately revised.

P/N T-1257 5727/A - ACTUATOR, LANYARD

The concept drawing on this actuator was approximately 90% complete. The first review of the design was in progress at the time of contract termination. Although the weight analysis of this actuator had not been updated for the then current design, its estimated weight was near its weight budget and no further weight reduction was anticipated.

P/N T-1257 5728/A - ACTUATOR, LOAD POSITION

The concept drawing for the load position actuator was complete and the design was in process of a fabricability review at the time of contract termination. Although the weight analysis of this actuator had not been updated for the then current design, its estimated weight was near its weight budget and no further weight reduction was anticipated.

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P/N T-1257 5729/A - ACTUATOR, INERTIAL RAMMER

The concept drawing on this actuator was completed and the assembly drawing begun. An internal design review of fabricability and assembly potential problems was in progress. The design of this actuator permits extensive flexing in its mounts and possible problems were being evaluated. The weight of this unit exceeds its budget, therefore, further weight reduction effort is anticipated.

4.0 Performance Analysis:

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An analysis of the static and dynamic performance of the hydraulic systems for elevation and traverse was planned for this program, but was suspended midway through the program so that available resources could be applied to the basis design of the components. Initial results are provided in for the early configuration. No effort was expended and therefore no results are available which evaluate the fluid inertia effects incurred by operation of the hydraulic subsystems.

SECTION E/180

Table 1 - Drawing Submittal Summary

FMC Part Number	Nomenclature	YII Drawing Number	Rev	P A R T S	B R O K E N	F U L
T-1258 5712/B T-1258 5713/B	Actuator, Equilibration RH Actuator, Equilibration RH Intensifier, Pressure	01-60356 19-60004	A B C	1 1 1 -	2 2 -	- 3 2 2
T-1258 5714/B	Actuator, Traverse	01-60355	- А В	1 1 1		 - -
T-1258 5716/C	Actuator, Elevation	02–60156	- A B C	1 1 1	- 2 2	3 3 3
T-1258 5718/B T-1258 5719/B	Accumulator, C.recoil - RH Accumulator, C.recoil - LH	08-60149	- A B C D E F G	1 1	2 2	3 3 - 3
T-1258 5720/B	Accumulator Unit, Feed & Equilibration	08-60999	A B	1	-	- -
T-1258 5720-1/B	Cylinder Cylinder, Machine Piston End Cap, Gas End Cap, Fluid Position Indicator Housing, Indicator Bushing, Indicator Wheel, Indicator Shaft, Indicator Indicator	08-60156 08-40565 08-40564 08-40566 08-40570 08-40577 08-40573 08-40574 08-40575 08-40576	A B C D	1 1 1	2 2 2	3 - 3 1 1 1 1 1 1 1 1 1

Final Status Report FMC Hydraulic Component Design P.O. P68622-84-LWHD

March 13,1987 Page 7

Table 1 - Drawing Submittal Summary

FMC Part Number	Nomenclature	YII Drawing Number	Rev	P A R T	B R O K E N	F U L L
T-1258 5720-3/B	Accumulator, Feed	08–60150	A B C D	- - 1	2 2 - 2	- 3 -
T-1258 5721/B T-1258 5723/B	Actuator, Walking, LH, Front Actuator, Walking, RH, Front		A B C	- 1 1 -	-	2 2 2 2
T-1258 5722/B T-1258 5724/B	Actuator, Walking, LH, Rear Actuator, Walking, RH, Rear	02–60155	A B C	- - 1	- -	- 2 2
T-1258 5725/A	Actuator, Breech	02-60160	- A B	-	- - -	2 2 2
T-1258 5726/A	Actuator, Auto-primer	02-60158	- А В	- - -	- - -	- 1 1
T-1258 5727/A	Actuator, Lanyard	02-60159	_ A	- -	-	1
T-1258 5728/A	Actuator, Load Position	02-60161	- A		2 2	3
T-1258 5729/A	Actuator, Inertial Rammer	02-60151	- А В С	1 1 1 1	2	2 2 2 3

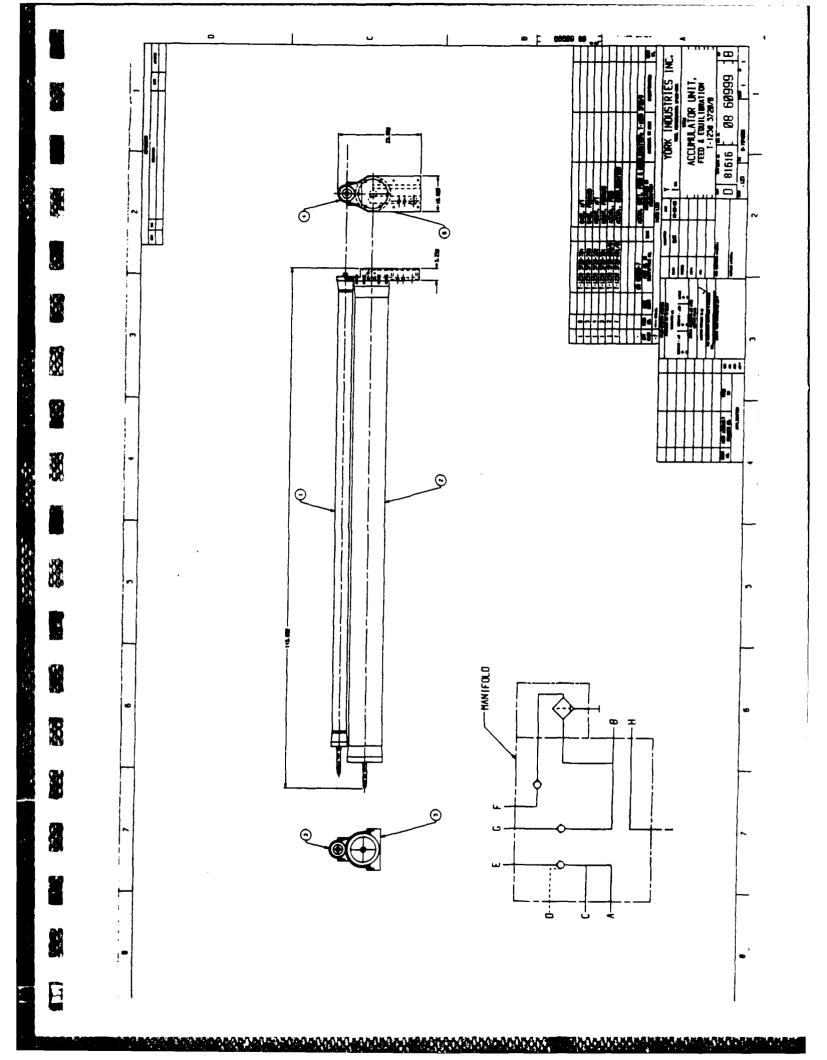
Table 2 - Hydraulic Component Weight Summary

FMC Part Number	Nomenclature	YII Part Number	Budget	Estimate
T-1258 5712/B T-1258 5713/B	Actuator, Equilibration RH Actuator, Equilibration RH	01-60356	135.00 135.00	110.14 110.14
T-1258 5714/B	Actuator, Traverse	01–60355	110.00	118.35
T-1258 5716/C	Actuator, Elevation	02–60156	44.00	36.87
T-1258 5718/B T-1258 5719/B	Accumulator, C.recoil - RH Accumulator, C.recoil - LH	08–60149	140.00 140.00	146.59 146.59
T-1258 5720/B	Accum. Unit, Feed & Equil	08-60999	36.00	43.18
T-1258 5720-1/B	Accumulator, Equilibration	08-60156	60.00	60.05
T-1258 5720-3/B	Accumulator, Feed	08-60150	70.00	68.57
T-1258 5721/B T-1258 5723/B	Actuator, Walking, LH, Front Actuator, Walking, RH, Front	02-60154	22.00 22.00	27.87 27.87
T-1258 5722/B T-1258 5724/B	Actuator, Walking,LH, Rear Actuator, Walking,RH, Rear	02–60155	22.00 22.00	26.34 26.34
T-1258 5725/A	Actuator, Breech	02-60160	5.00	4.00
T-1258 5726/A	Actuator, Auto-primer	02-60158	2.50	5.16
T-1258 5727/A	Actuator, Lanyard	02-60159	1.00	4.38
T-1258 5728/A	Actuator, Load Position	02-60161	35.00	33.78
T-1258 5729/A	Actuator, Inertial Rammer	02-60151	30.00	38.80
			1031.50	1035.02

DESCRIPTION: ACCUMULATOR UNIT ASSEMBLY

STATUS - PER YORK:

The newly defined port manifold was being added to the concept drawing of the Accumulator Unit at the time of contract termination. The mounting techniques for both accumulators had been defined and coordinated with FMC. The front slide mount carries both axial and radial loads. Slip joints are used at the mid-slide mount so that expansion of the accumulators does not load the slide; therefore, only radial loads are carried. The piston position indicators are located near the mid-slide mount. The YII request for an evaluation of readability of position indicators as shown by the concept drawing was still pending.



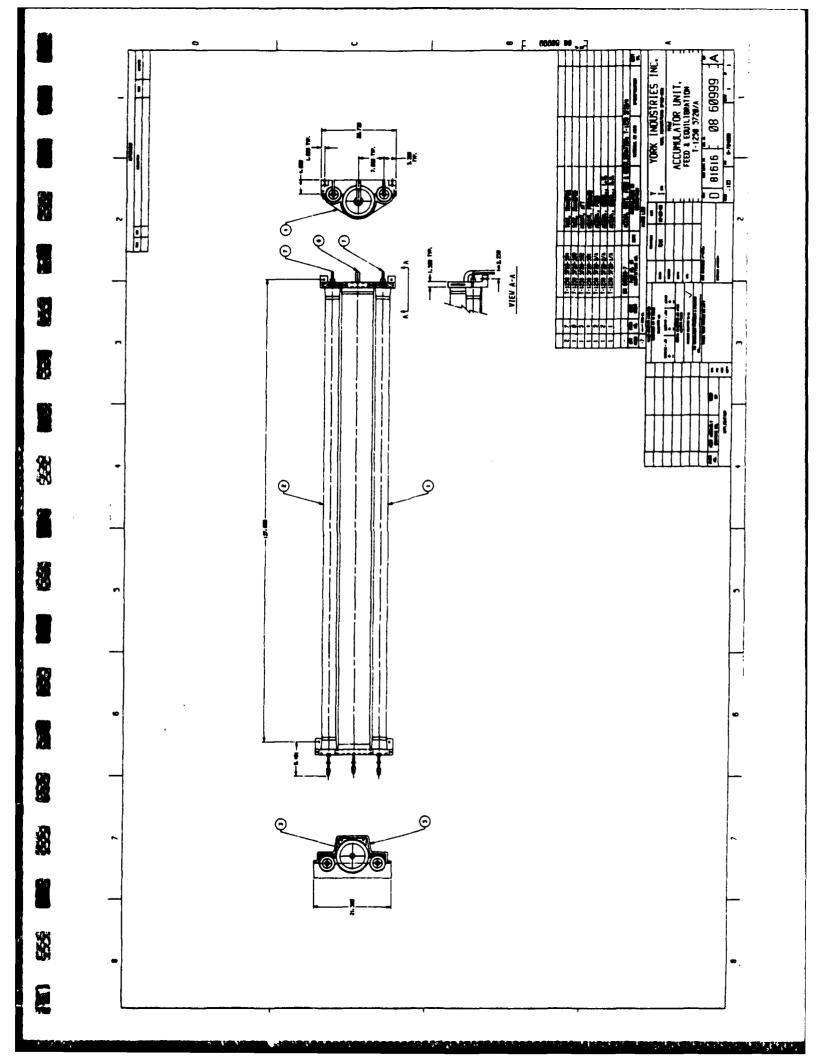
DESCRIPTION: ACCUMULATOR UNIT ASSEMBLY (Obsolete)

STATUS - PER FMC:

8

Port manifold addition (E/110) obsoleted this design. This manifold was added to facilitate circuit integration while improving reliability and durability.

AUTHOR: Jeff Ireland/Bart Anderson



DESCRIPTION: EQUILIBRATION ACCUMULATOR

STATUS - PER YORK:

The concept drawing of the equilibration accumulator had been completed and the assembly drawing was being revised to change the length of the accumulator to facilitate its mounting to the slide. This component meets its weight budget and was in fabricability review. The length of the cylinder of this accumulator was set by the need to match the length of the Feed Accumulator as a means to minimize overall system weight, however, this length forced this component into the list of long lead items being prepared at the time of contract termination.

95109 80 YORK INDUSTRIES INC. 5 HYDRAULIC ACCUMULATOR, EQUILIBRATION T-1258 5729-1/C CAMBOLFILLED THE 60156 PENCHE 852-CL/865H MODRALLIC ACCID. COUR. IBBATION 1-1259 3729-1/C medica.NMI in the same occasioning. SEAL BING WAST, INBUST WESTING, INDUSTRIC CHEE SPRING 80 CARLE ATTACH # 0-784BB CIL HOER NOICATOR 81616 PUSITION INDICATOR ASSI 80 MESSE-7 80 4073-7 27822-118 81 AFT 36703 FITTING, CAS PORT DIO CAP, GAS
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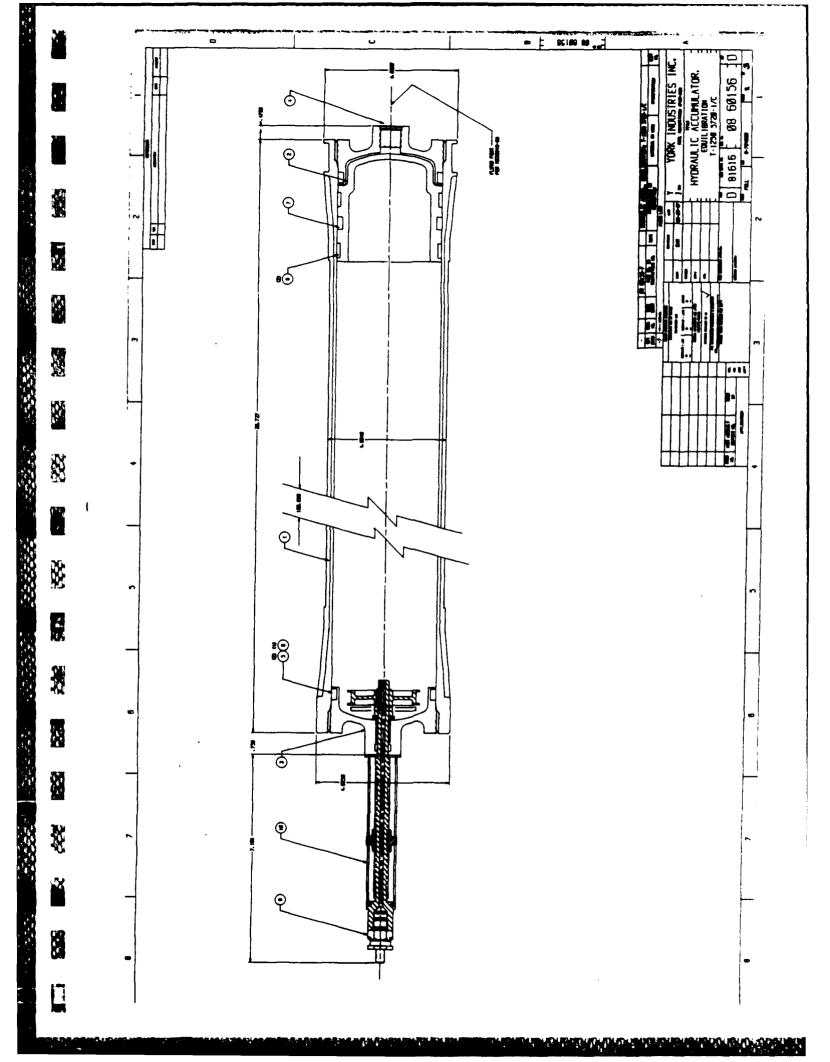
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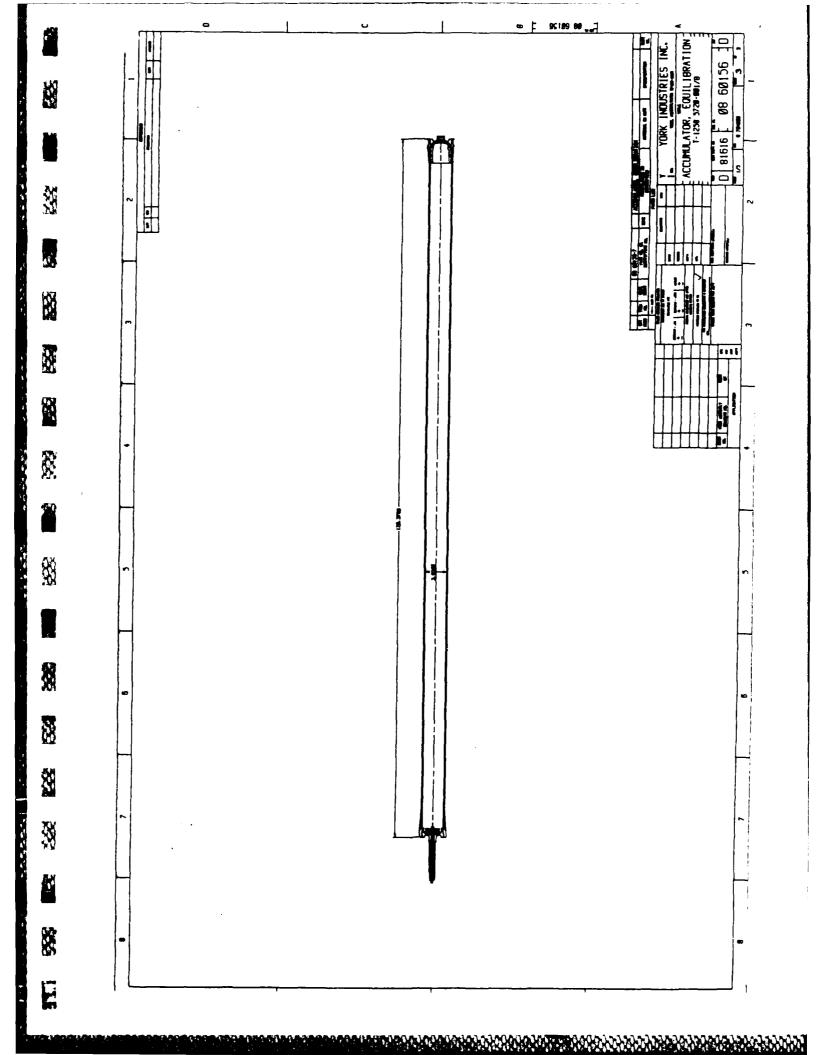
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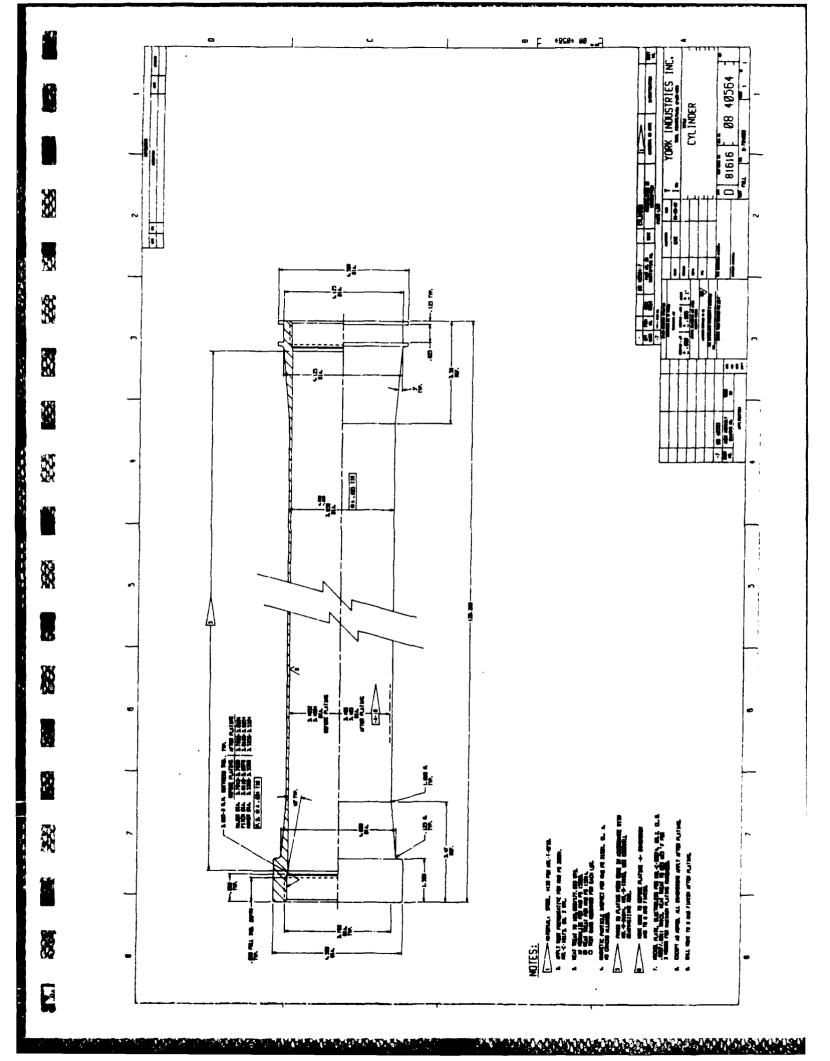
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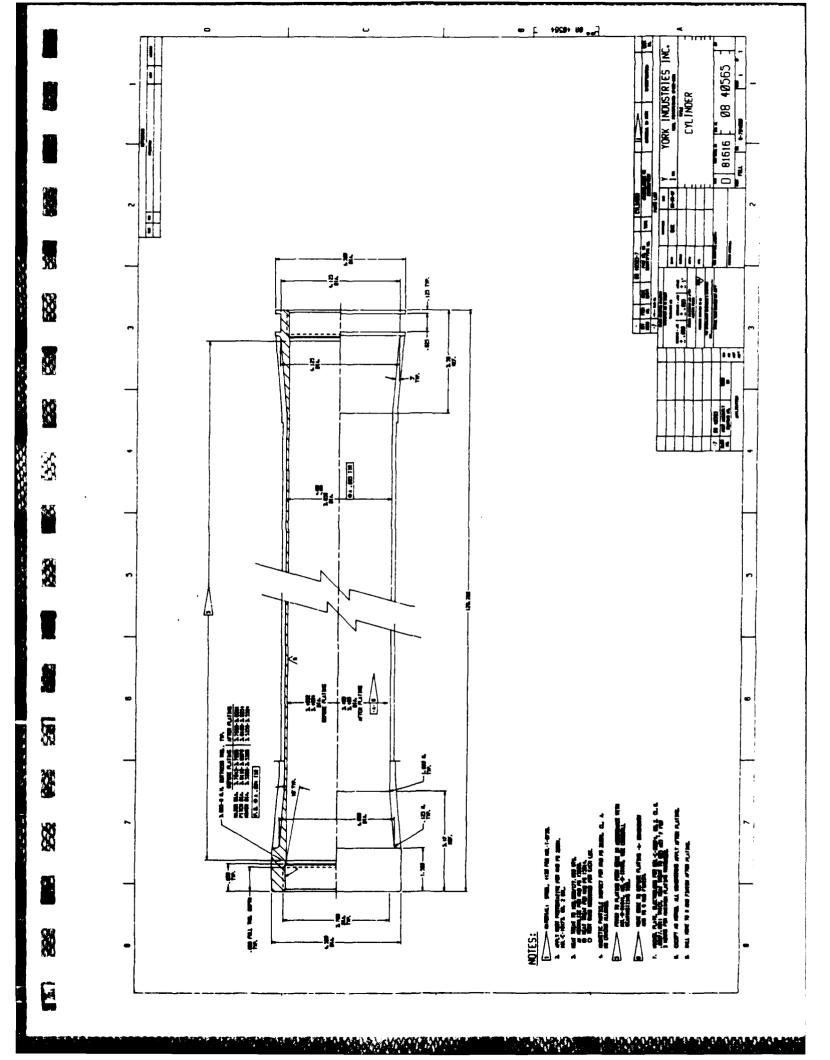
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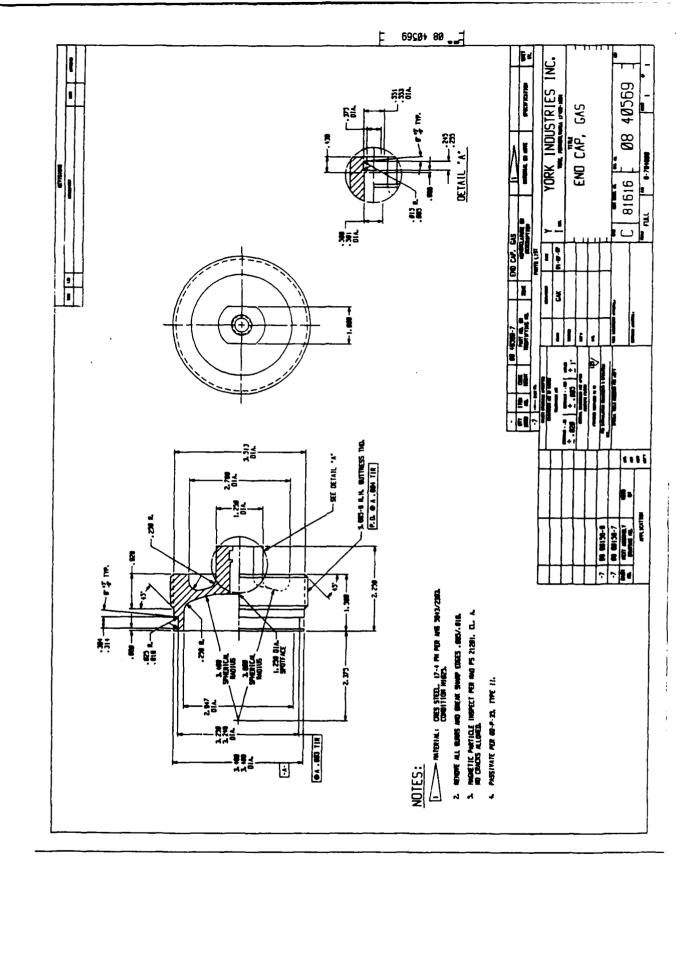
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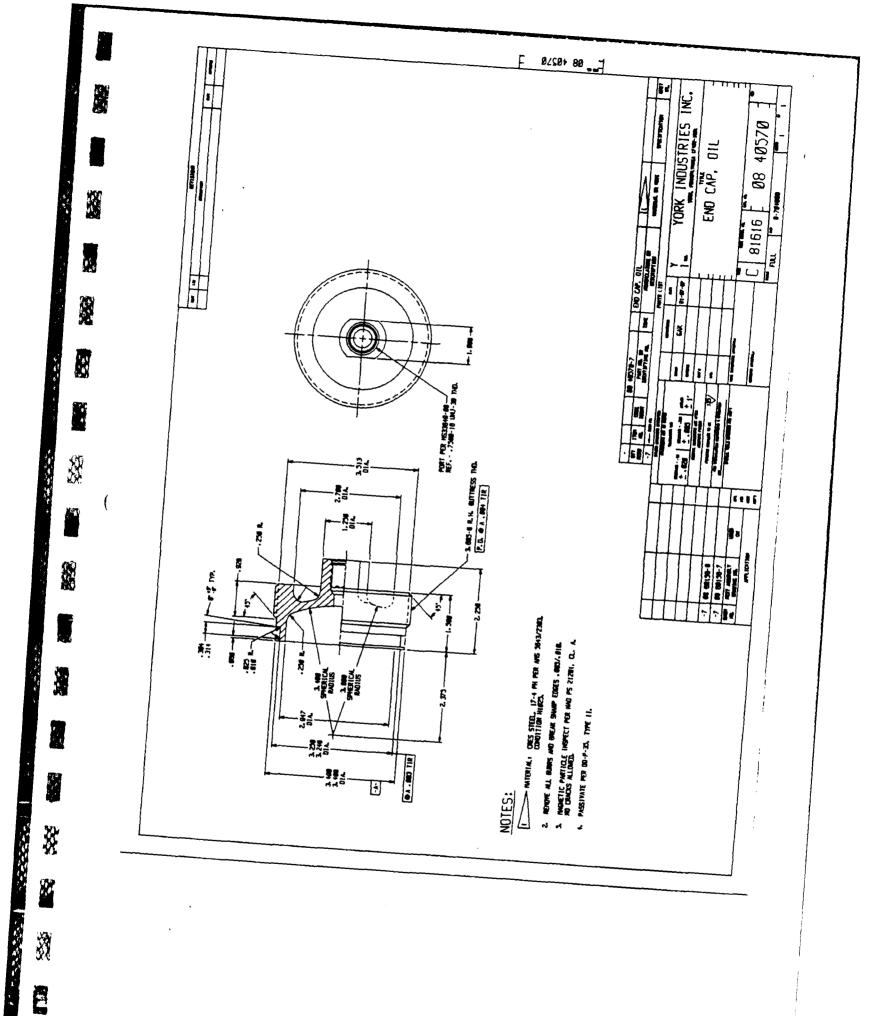


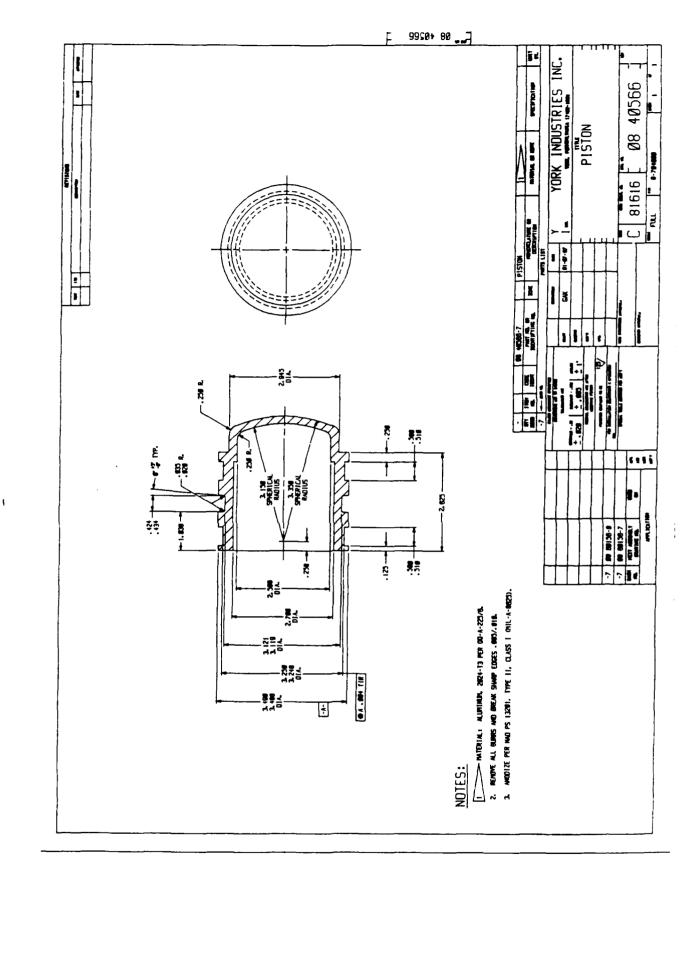






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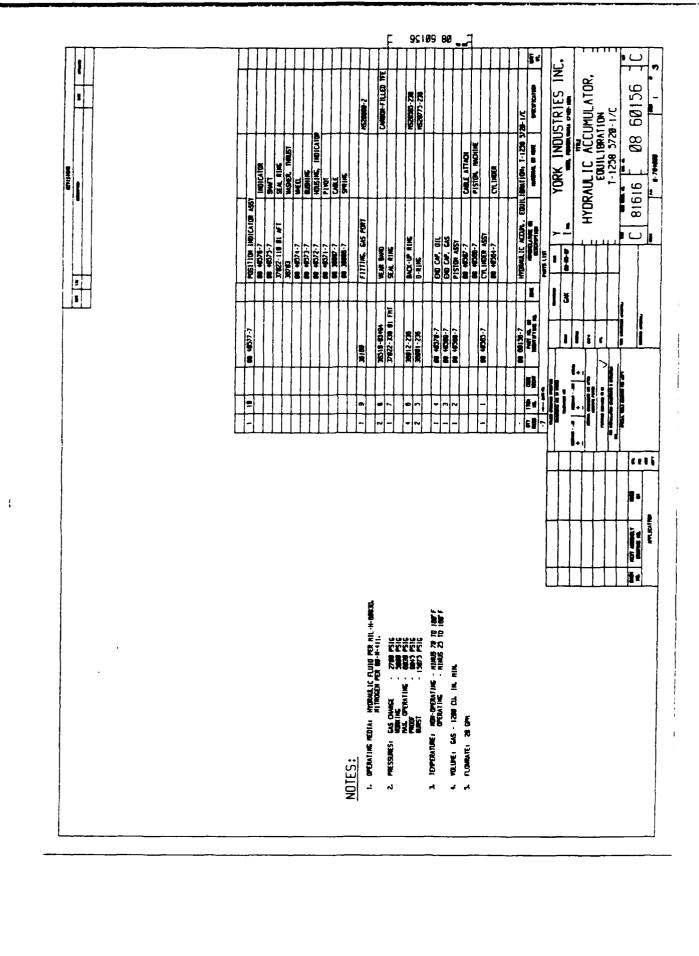
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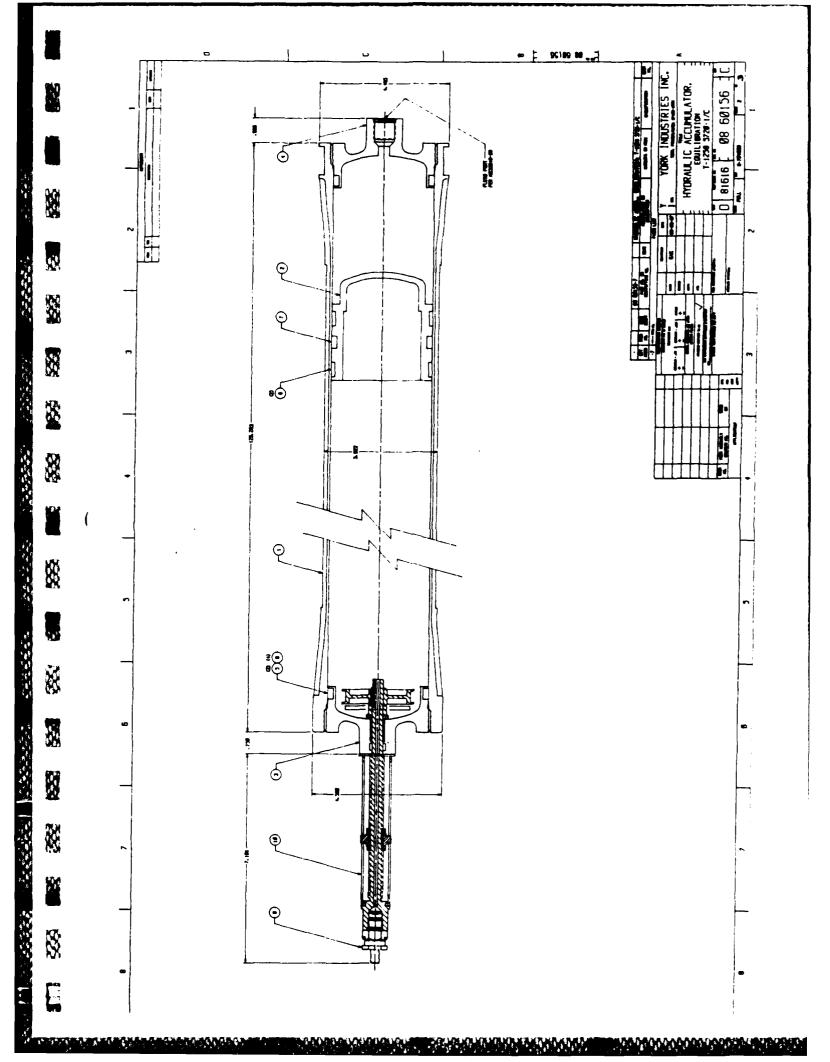
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GENELAM 6 SCA, RING MADER, PRINST MEDIA MEDIAG, INDICATE PINGI 88 CALL ATTACH **BICATO** 3 91918 FITTING CAS PORT ں DE CA. DIL DE CA. GAS P1570A ABSY DE 40500-7 TOL IMBUR ABSY DE 40500-7 BACK-UP RING 0-RING KA BOD 1 6 FEE .. FEE 9 1 3 K 60 4000 H 822-1008E /- COCD+ M 1 1 1 1-11CD+ 10 -= i 1. 1. OPERATING MEDIAN MYCHARILIC FLUIG FOR HILL-H-GREEN, HITMOZEN PER 68-41-411. PODATIS - NIMB 20 10 100 F řřěřř **RRB**S<u>Ř</u> WELDER GAS - 1288 CIL IN, RITH. CAS COMES WARRIST WA. O'CONTING : FLOWNTE: 28 DM TENTERN TURE THE STREETS: NOTES: J

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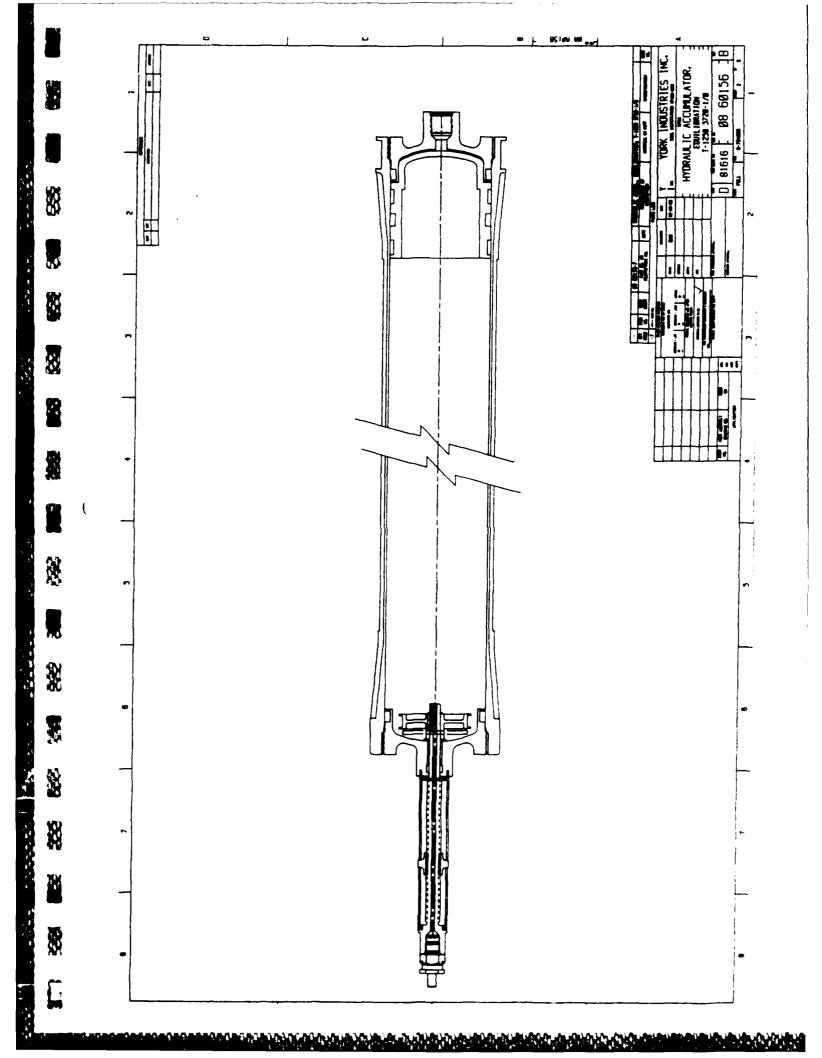
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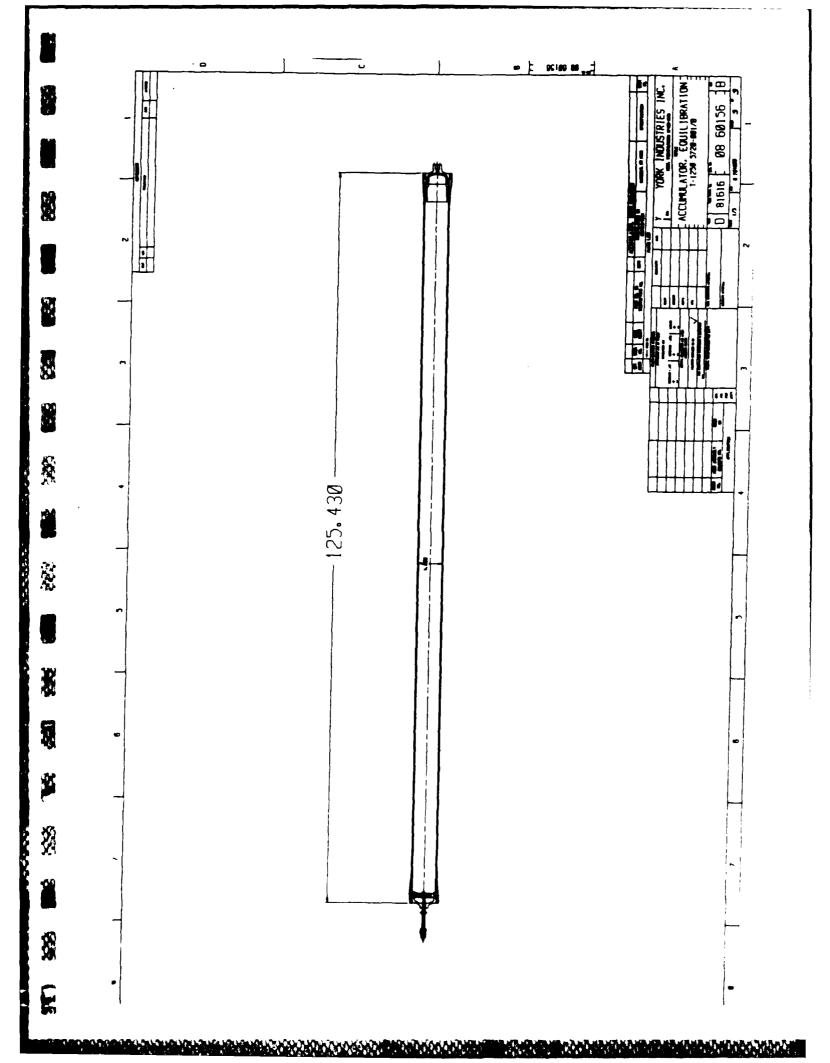
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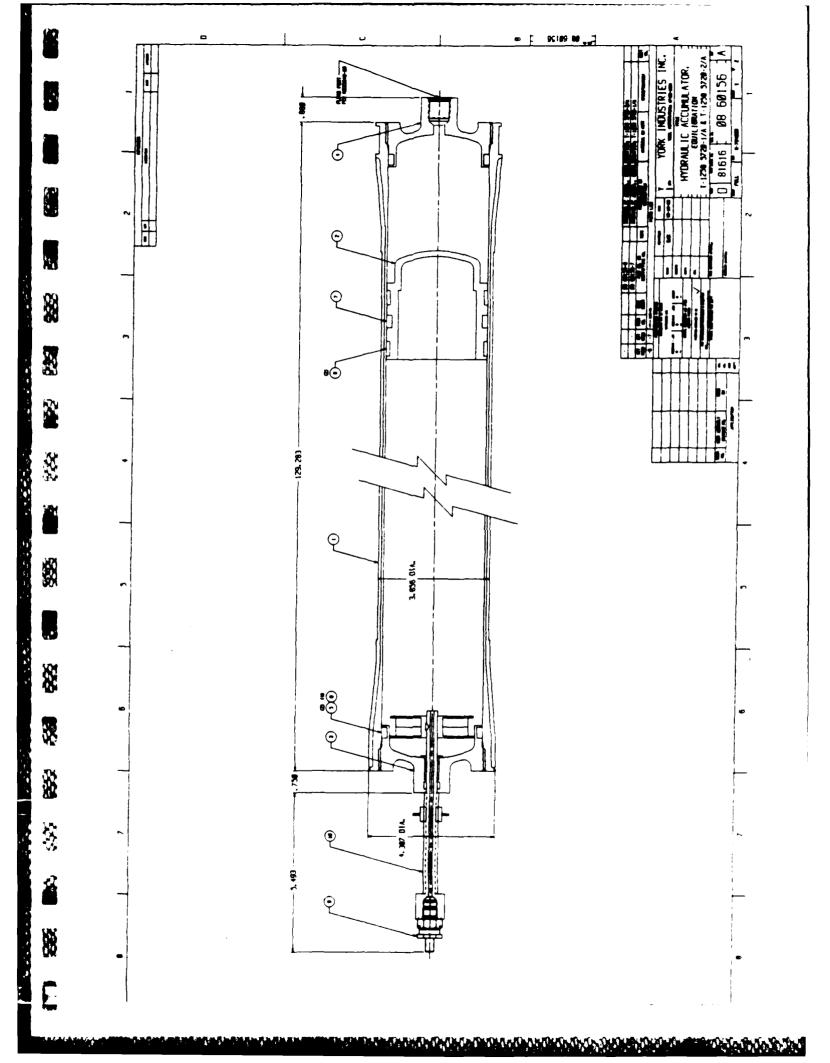
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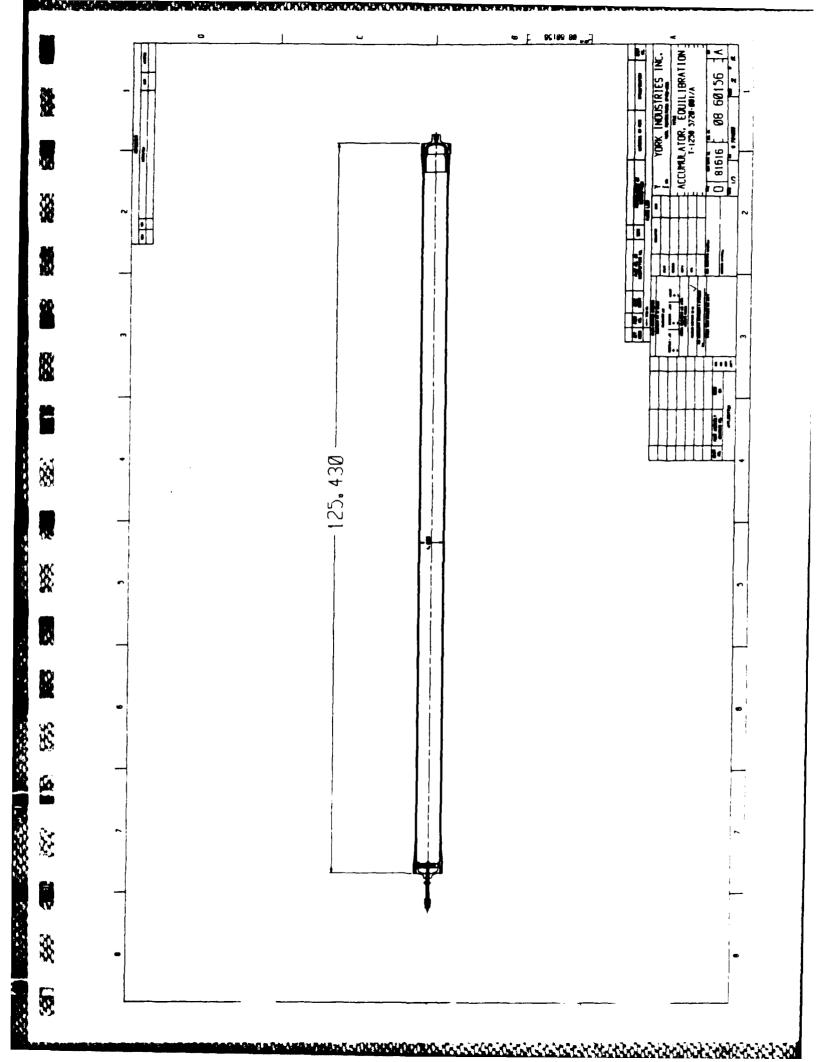
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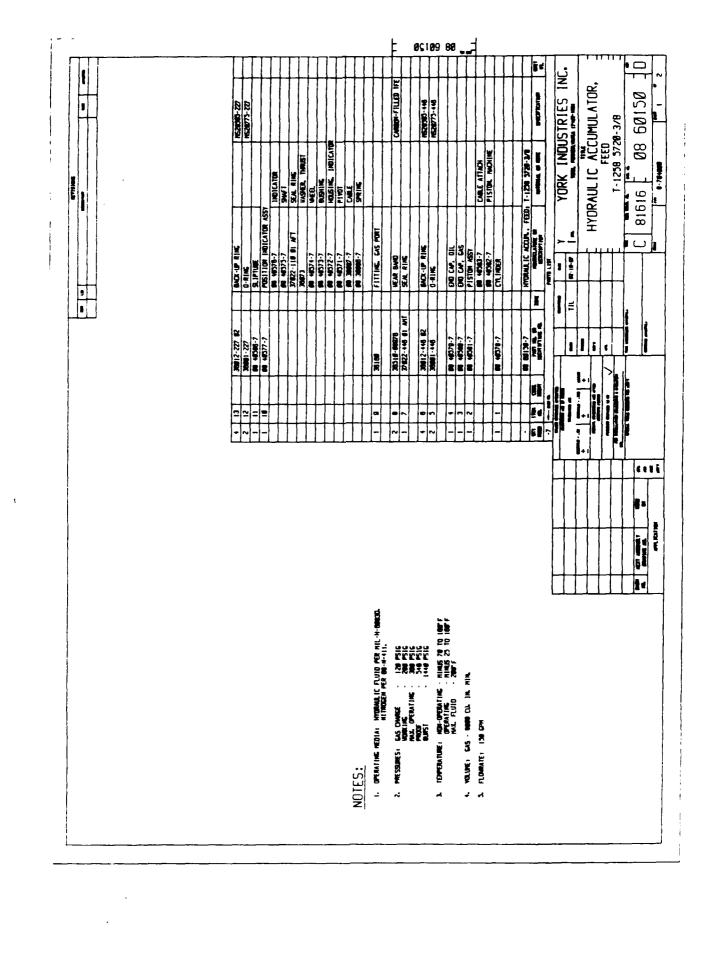




DESCRIPTION: RESERVOIR ACCUMULATOR

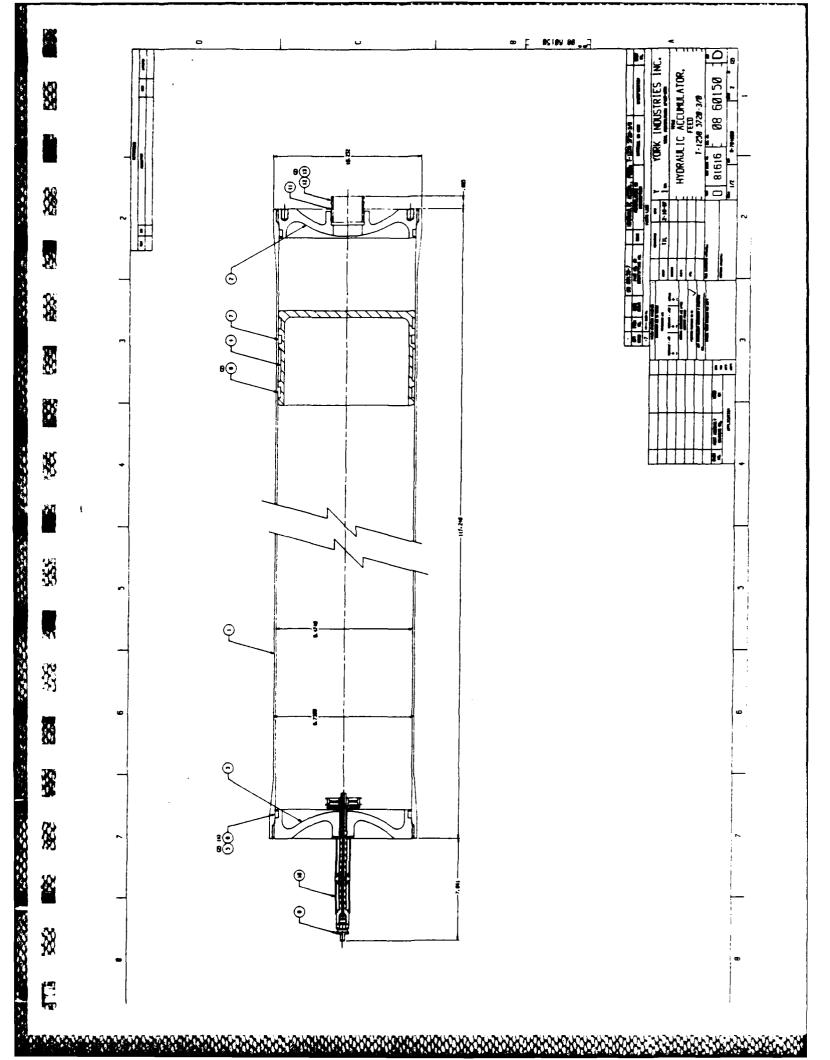
STATUS - PER YORK:

The concept drawing for the feed accumulator is complete and the assembly drawing was being revised to change the length of the accumulator to facilitate its mounting to the slide. This component meets its weight budget and was in fabricability review. The length of the cylinder of this accumulator was set by the need to match the length of the Equilibration Accumulator as a means to minimize overall system weight.

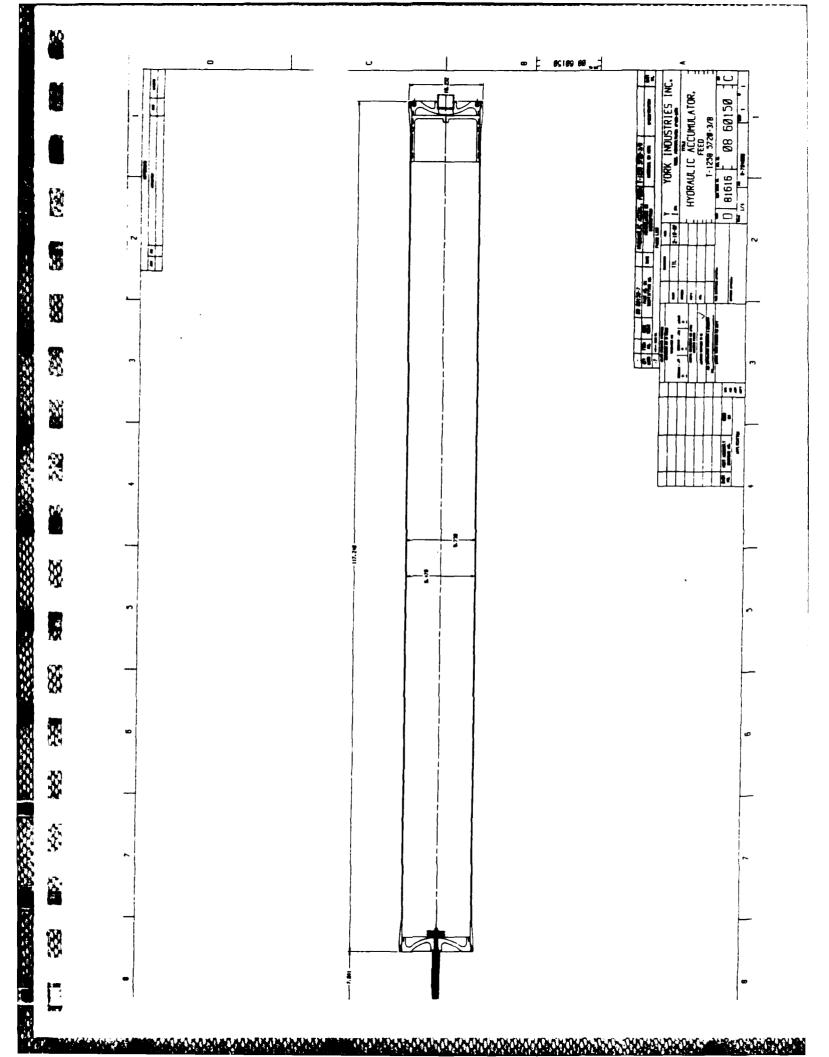


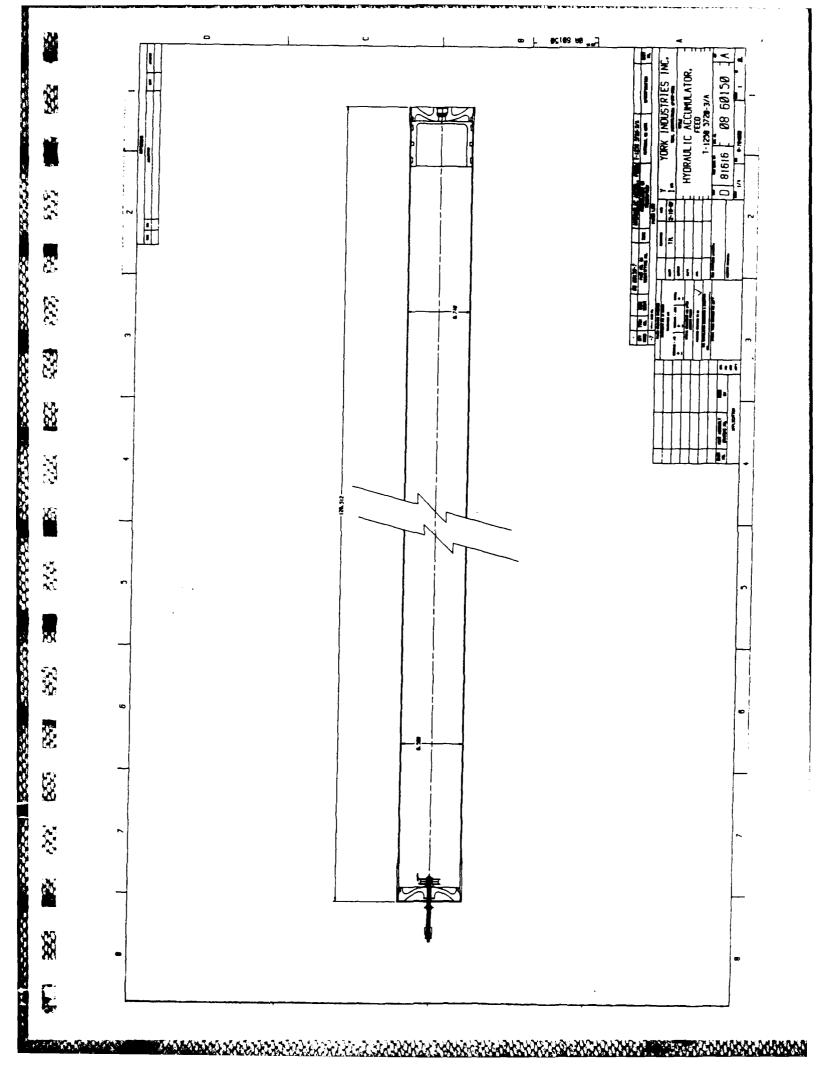
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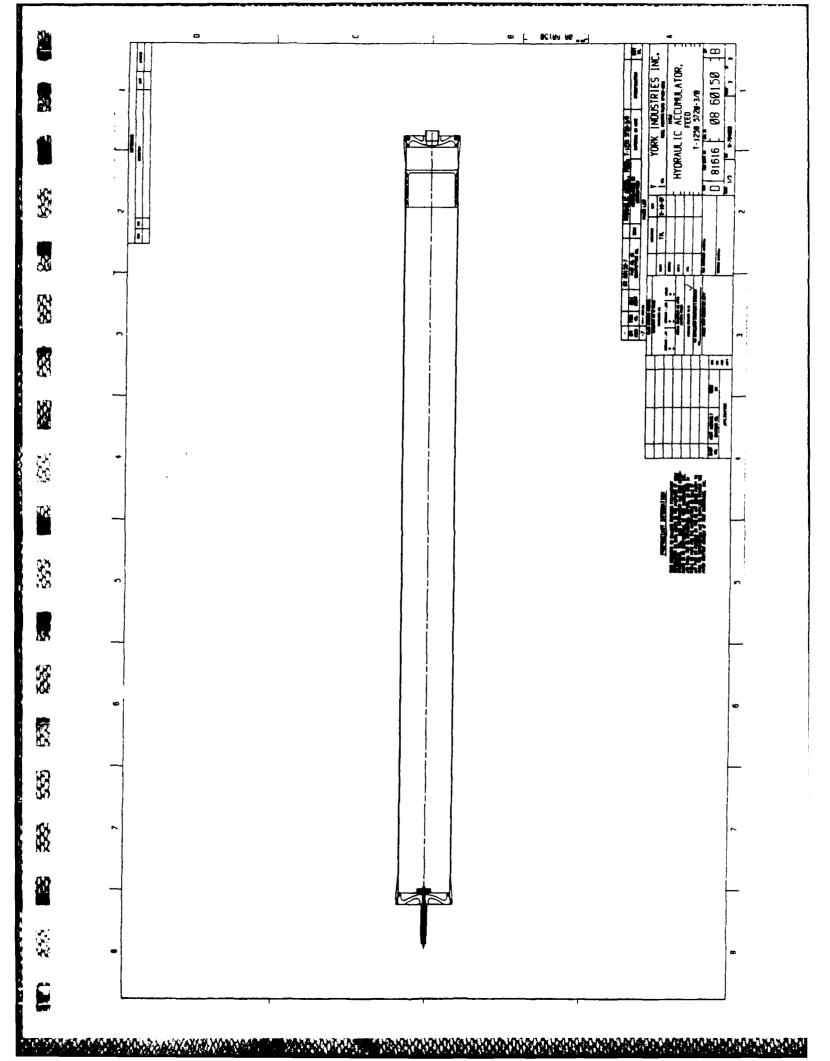
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DESCRIPTION: RESERVOIR ACCUMULATOR (Obsolete)







DESCRIPTION: BREECH ACTUATOR

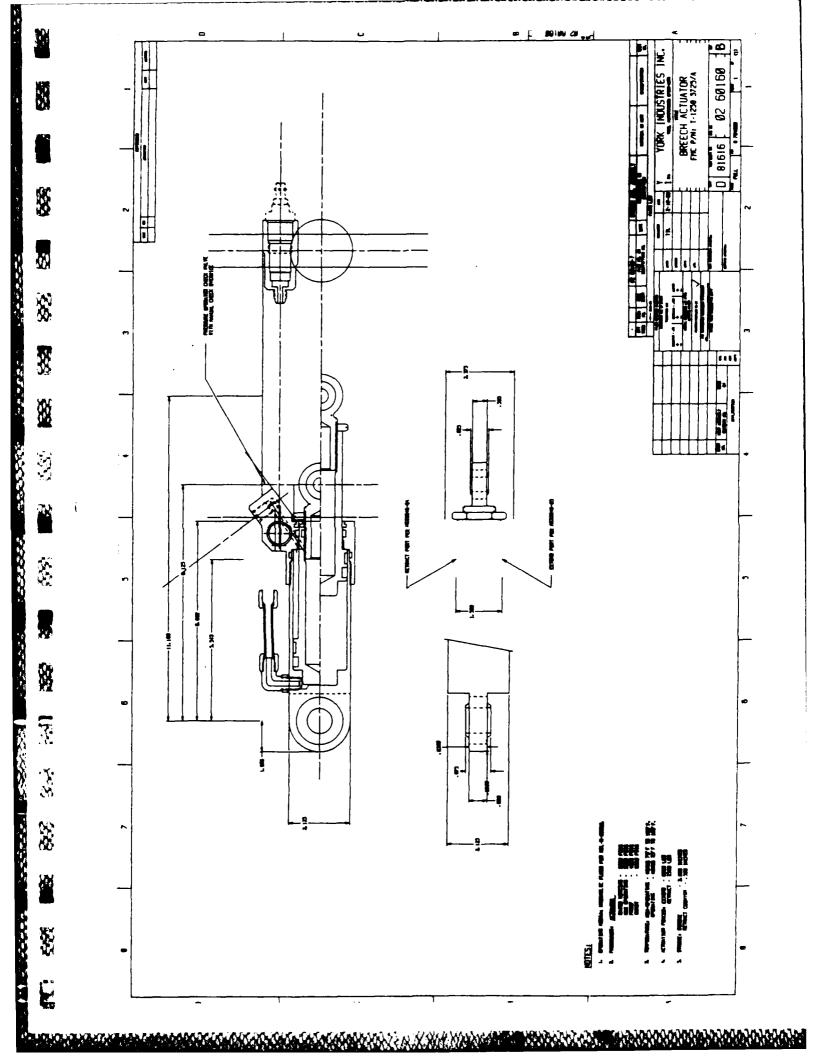
STATUS - PER YORK:

The concept drawing for the Breech Actuator had been completed and the assembly drawing was being revised to incorporate a check valve and FMC specified port locations. The pilot-operated check valve provides an extended stroke position lock when hydraulic pressure is removed from the unit. This unit meets its weight budget and no further weight reduction is required.

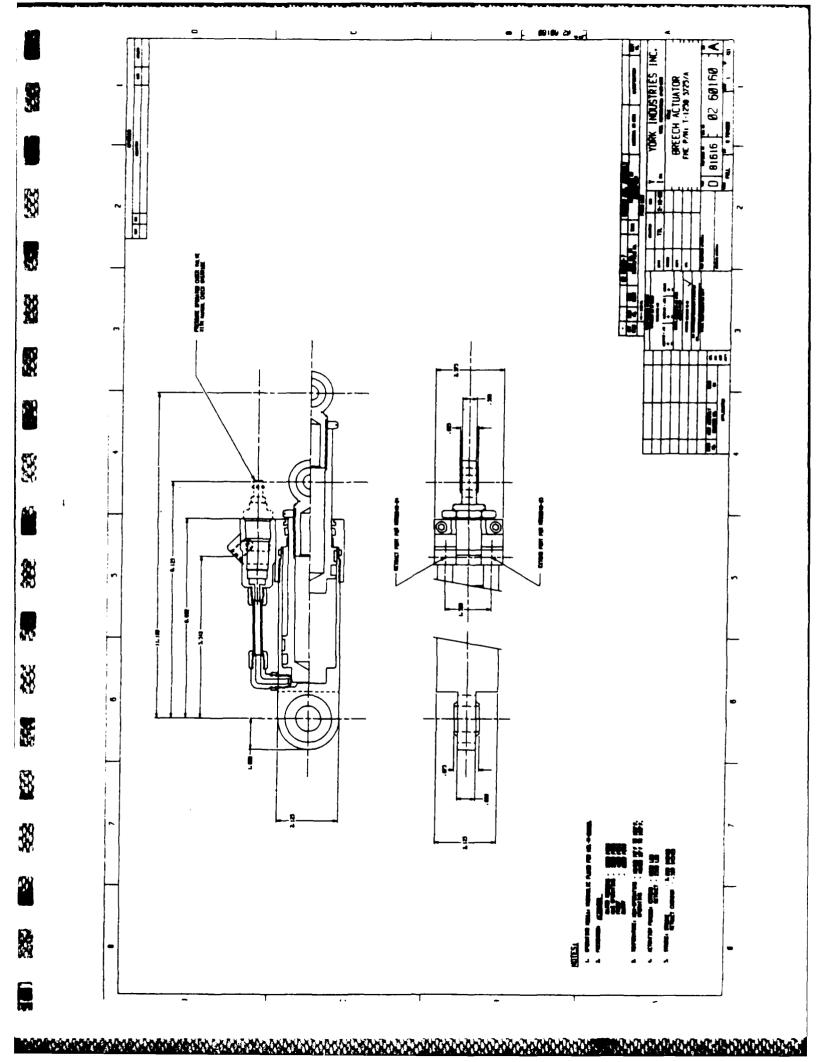
STATUS - PER FMC:

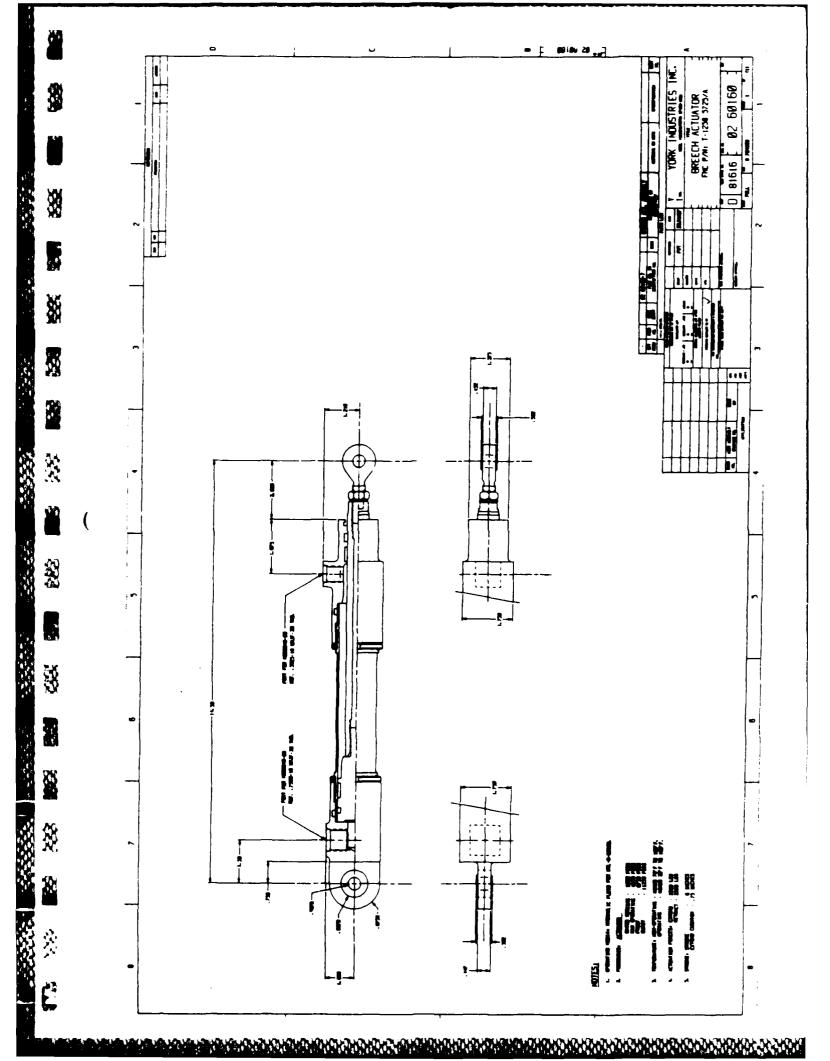
The pilot-operated check with manual override prevents accidental breech closure due to hose failure and facilitates manual opening and closing.

AUTHOR: Jeff Ireland/Bart Anderson



DESCRIPTION: BREECH ACTUATOR (Obsolete)





DESCRIPTION: COUNTERRECOIL ACCUMULATOR - Left

STATUS - PER YORK:

The concept drawing for the left and right accumulators is approximately 90% complete; however, the increase in volume from 1600 cubic inches to 2400 inches drives its estimated weight above the target weight by a significant amount. In the interest of weight reduction, it is recommended that the factor of safety on maximum operating pressure for proof pressure be reduced from the standard value of 2.0 to a value of 1.5 and that the burst factor be reduced from 4.1 to 3.0 on the cylindrical section only. Design factors of safety for the end caps and threaded joints remain at the standard level of 4.0. FMC approval was obtained at the March 6, 1987, coordination meeting.

STATUS - PER FMC:

The volume increase was to accommodate the broad temperature range coupled with varying amounts of energy in storage (see C/120).

AUTHOR: Jeff Ireland/Bart Anderson

61109 88 -3 6 -HYDRAULIC ACCUMULATOR, EMERCY STORAGE T 1258 5718/8 & T 1258 5719/8 YORK INDUSTRIES INC. 08 6/1149 BACK RANGE HYBINA IC ACDIA, DEBAY STBACE, 1 128 STEAM HYBINA IC ACDIA, DEBAY STBACE, 1 128 STEAM BY BENEVAL OF THE WAY OF RUBHING HOTCATO MUSING HOTCATO PLYOT CARLE ATTACH STAL BIRG WASHER HALLST WEED. 3 MELCATE SEW 1 81616 251119 101111 1011 FITTING CAS PORT RING, METAINING BOX -UP RING 0-RING DOX -UP RING 0-RING 0 8145 0 8145 510° P1510H END CAP. EAS P1570H ABST BN 6810H 7 BN 6810H 7 CYL 100ER ABST BOX UP RING . . ME A BAND SEA. P. P. 1 †**E**_1 1 3 60 6600 7 60 6600 7 7 6600 7 / L/Q. . 1 1 1 - VECTO - 1 / 120m NO. 2 2 2 2 -2 = = = 68-.... . i 1. OPERATING MEDIA: MYSTAMALIC PLUID PER HIL-H-GARDEN. HIL-H-GARDEN. HIL-H-CALLIN. THINGS NO THE LOW ! #5#5# #5#5# #5#5## 545 - 278 OL IN NIK OCCUPATION OF THE PARTY OF THE CAS OMER WEREIN, PAS, OPERATING PROST FLOWBATE: TRO GPH 100 CRATURE: PESSON S. M. UM. NOTES:

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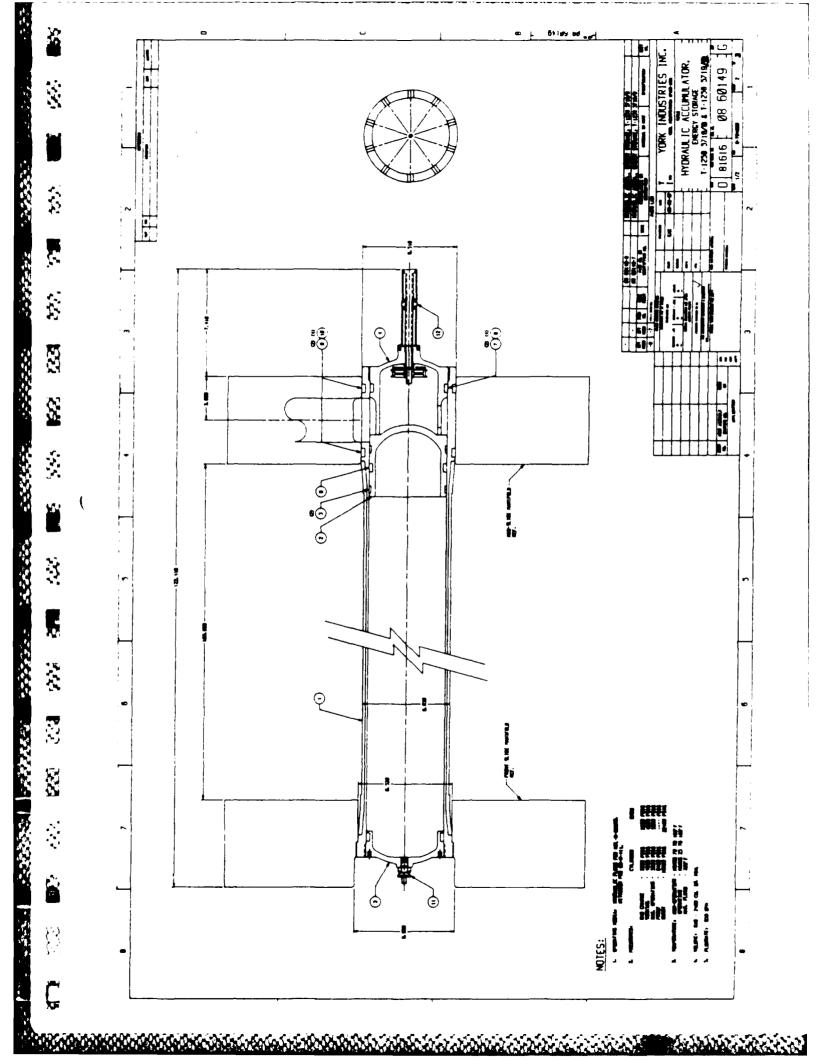
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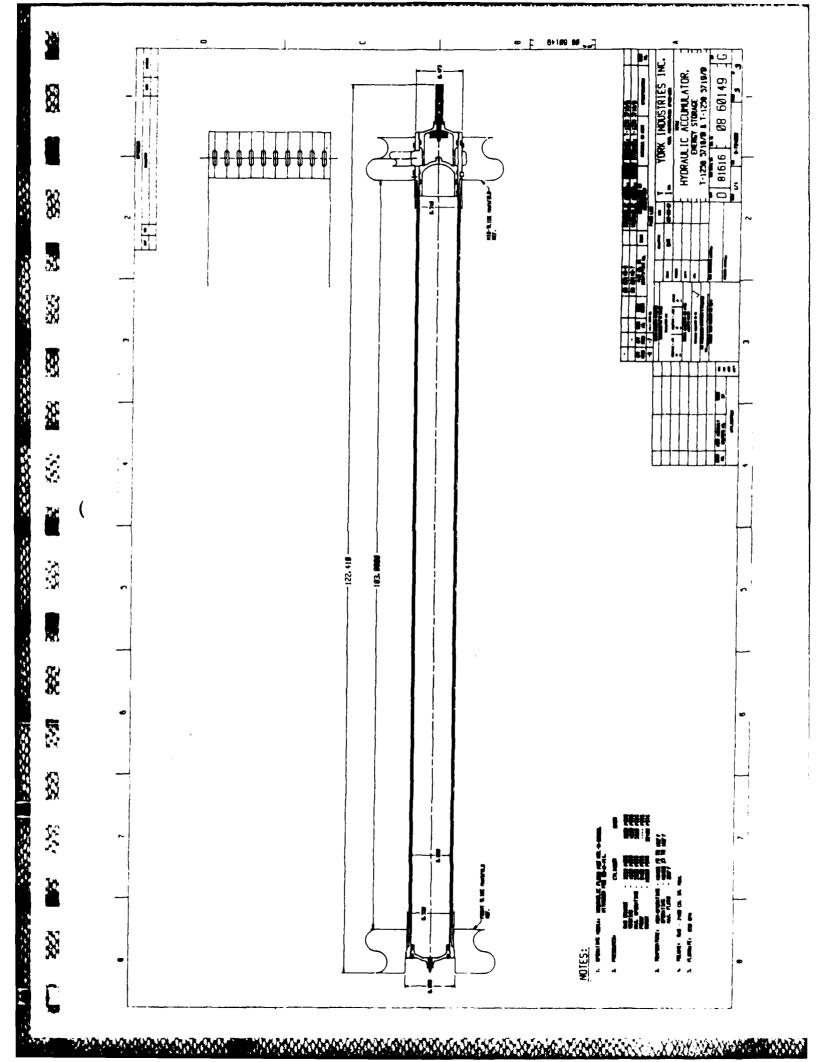
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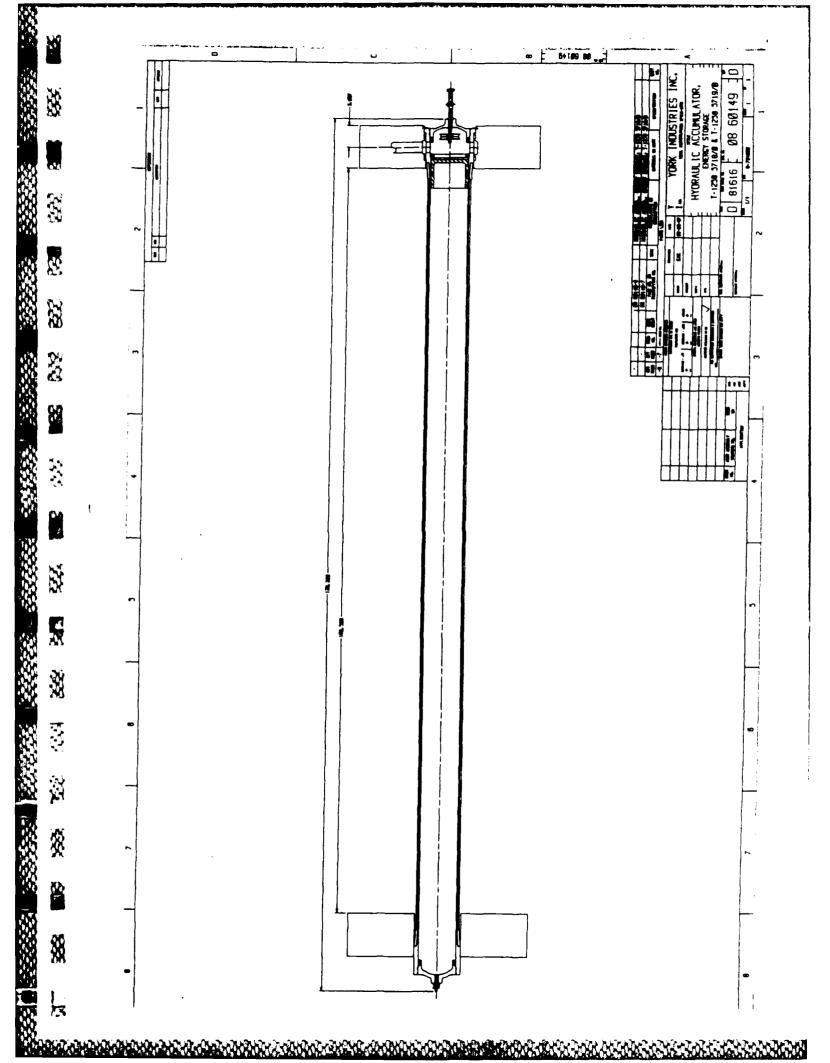
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STATES OF THE STATES





DESCRIPTION: COUNTERRECOIL ACCUMULATOR - Left (Obsolete)



5+109 80 Θ YORK INDUSTRIES INC. HYDRAUL IC ACCUMULATOR, ENERGY STORAGE T-1258 5718/8 & T-1258 5719/8 60149 1 HTDRALL C ACCUS., EREGY STOUGE, 1-120 37 IA-4
HTDRAL C ACCUS., EREGY STOUGE, 1-120 37 IA-4
HTDRAL C ACCUS., EREGY STOUGE, 8 HT PROSCAME & MARIA & HT PROSCAME OF P 80 BUSHING INDICATOR CARLE ATTACH PISTON, MONINE 8-78-488 CALINDER RVISION. 91616 PUSTITION INDICATOR ASST 88 48378-7 FITTING, GAS PORT RING, RETAINING CPL INDER ASST STOP. P1STON
END CAP. OIL
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68 46XXX.7 0-RING BACK-UP RING D-RING BACK-UP RING O-RING BACK-UP RING O-RING BACK-UP RING WE'NE BAND SEAL RING 3 20 (50) 49-0 20 (49-7 7401 49-7 14001 97-116-116 60 46001-7 60 46001-7 60 46001-7 60 46001-7 7 - YOU'S FB 44001-7 1 | 1 | i 7-7759+ 80 ť 100 = feti The second 1. OPERATING MEDIAL HYDRAGLIC FLUID FOR MIL-H-ORNERS. MINGGEN FOR 809-H-411. NON-OPERATING - RINGS 78 TO 100°F OPERATING - RINGS 23 TO 100°F NAX. FLUID - 273°F 6.45 DAMR - 388 PSIG MORCHG - 438 PSIG MAL OPERATING - 738 PSIG PMODF - 11238 PSIG BLRST - 38888 PSIG VOLUME: GAS - 2239 CIL IN HIM. PLOWRATE: TRO GPM TEMPERATURE PRESSURES: NOTES: ~

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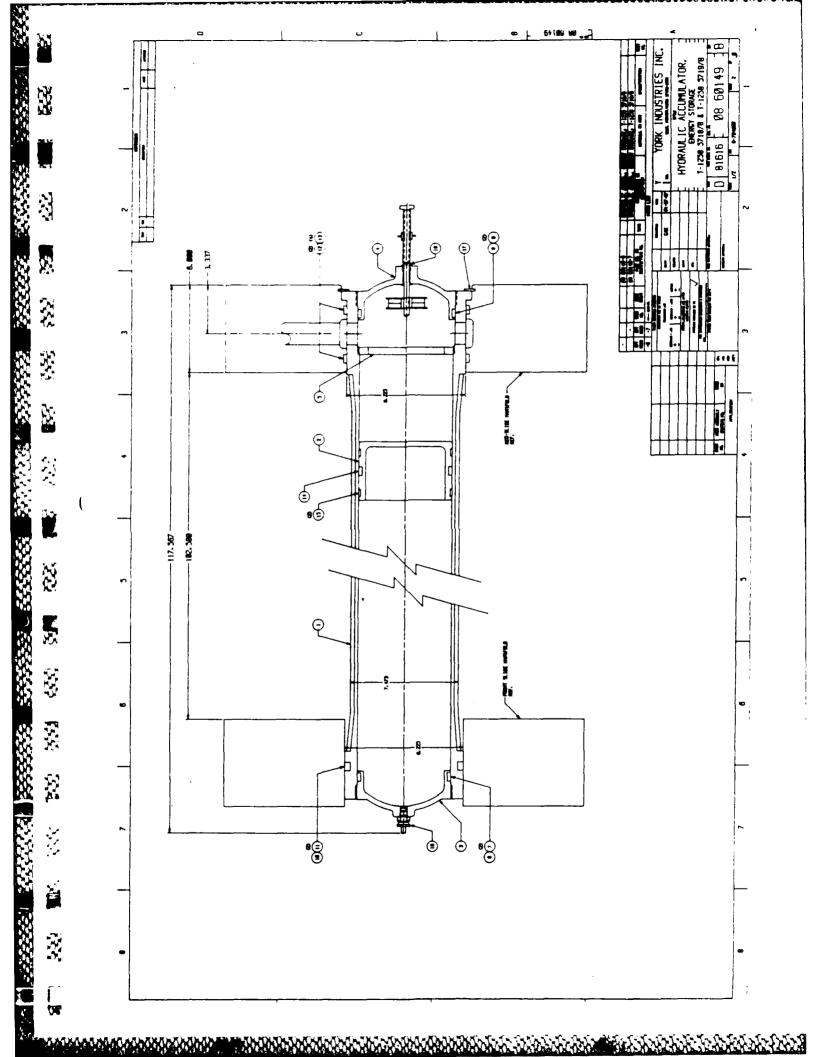
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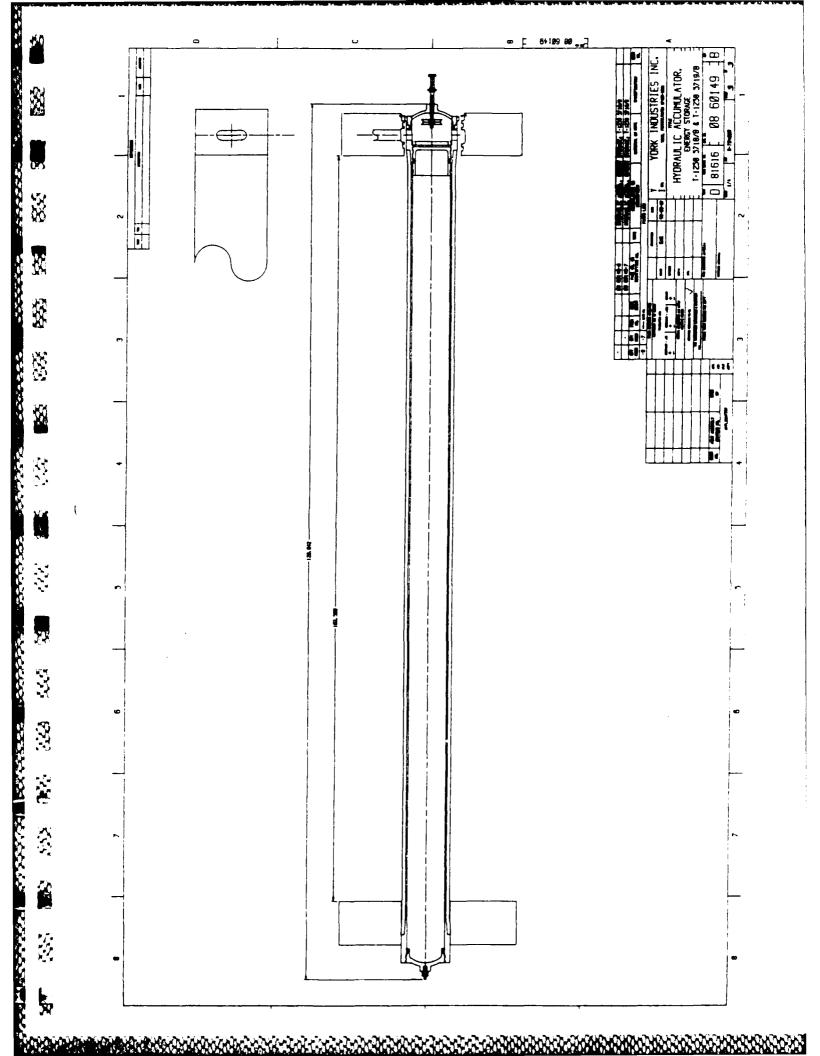
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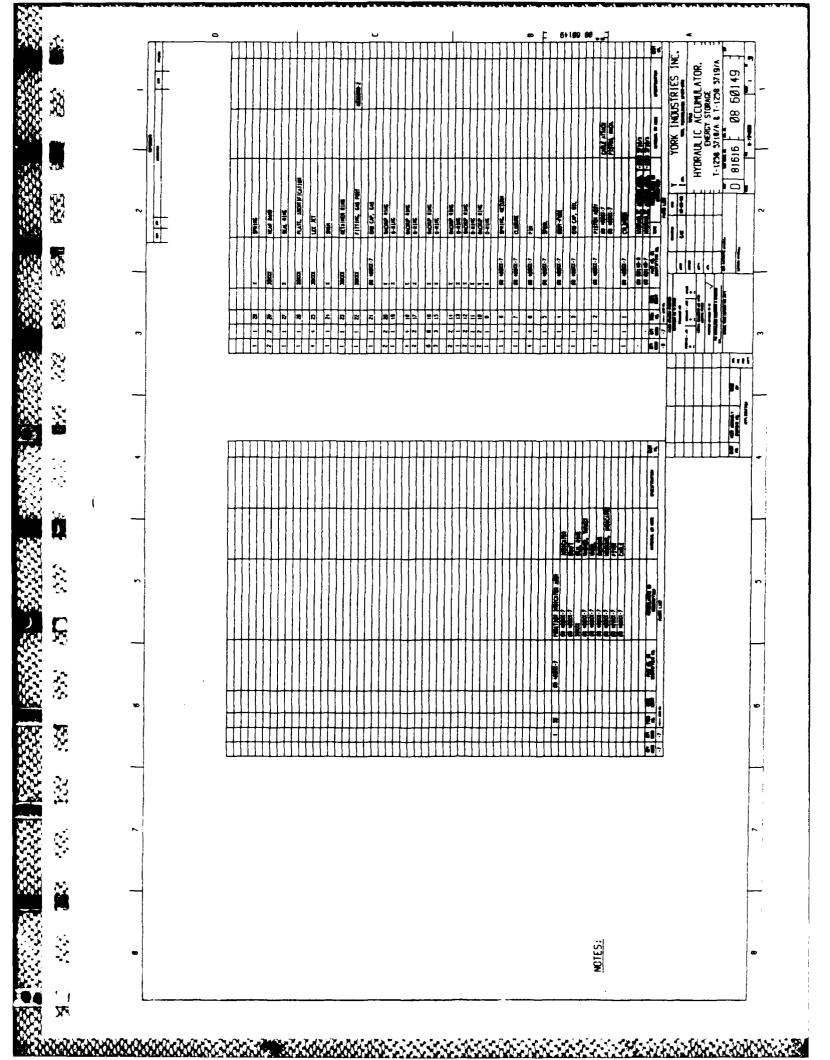
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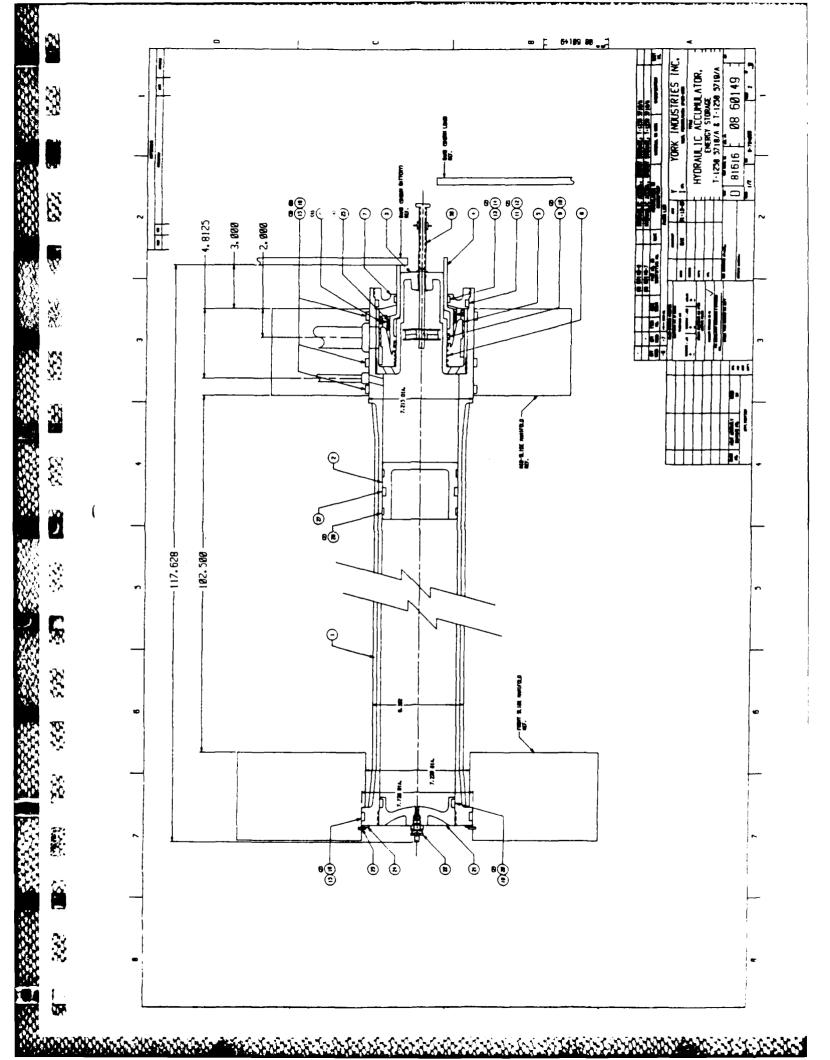
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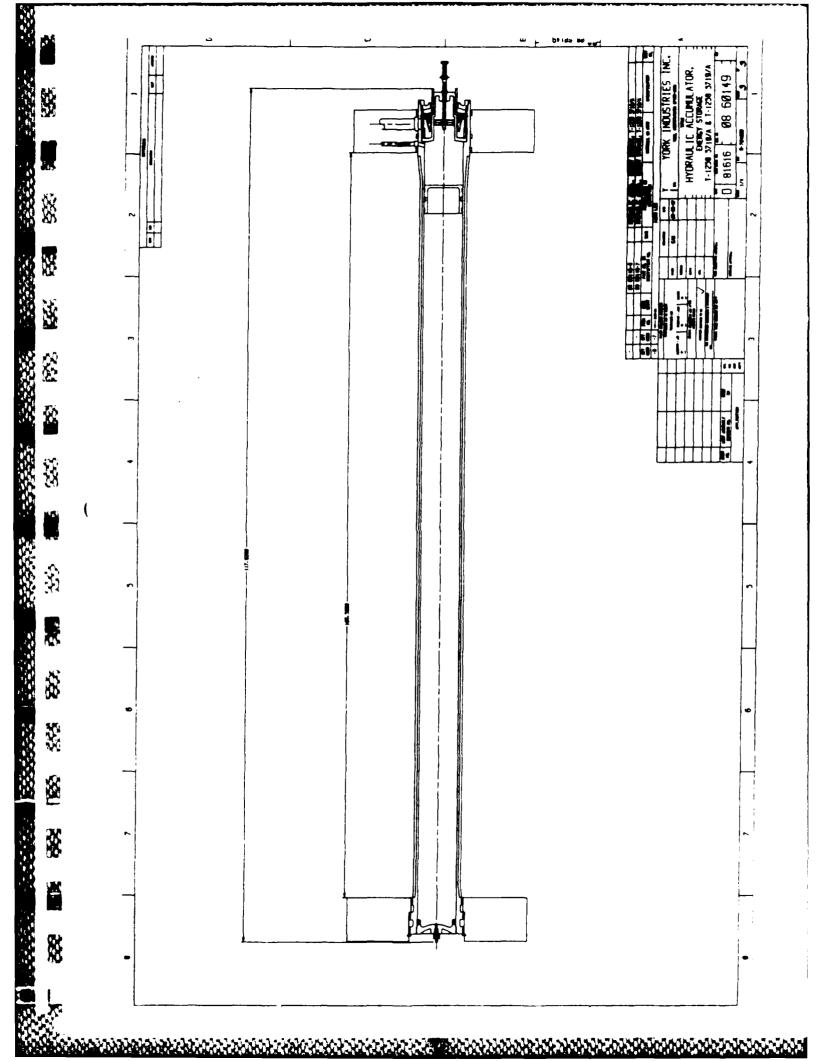
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DESCRIPTION: COUNTERRECOIL ACCUMULATOR - Right

STATUS - See E/150

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DESCRIPTION: ELEVATION ACTUATOR

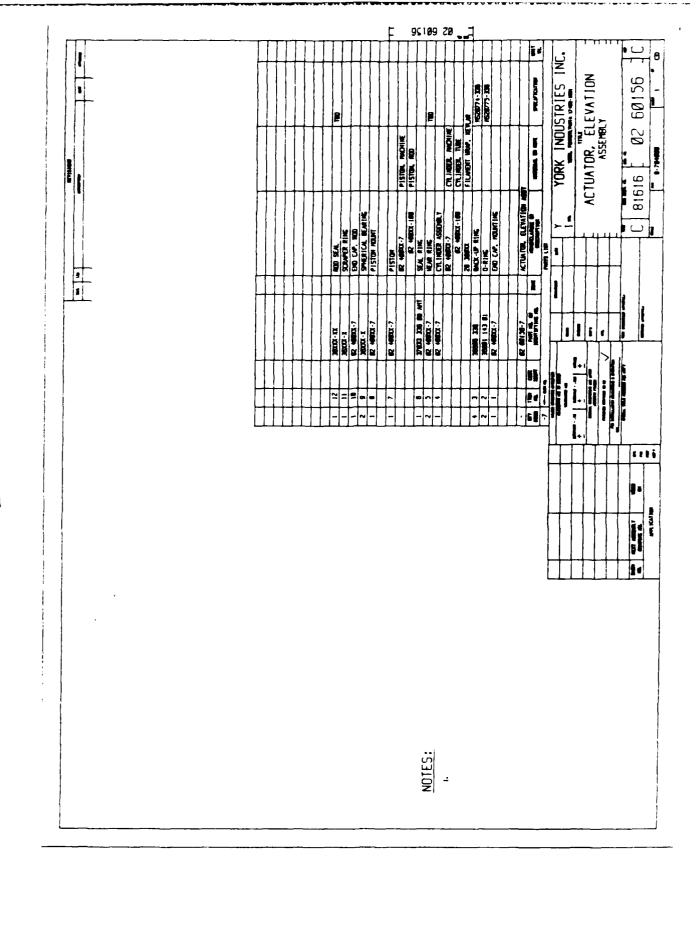
STATUS - PER YORK:

A single actuator, attached to the center of the slide, was substituted for the original one on each side and the stroke was lengthened. The concept drawing for the revised stroke was completed and was in review or fabrication evaluation. The project weight of this actuator meets its weight budget; however, further reduction was planned to allow for the weight growth in the Counter-recoil Accumulators as previously discussed later. Tailoring of cushioning at end of stroke is planned whenever the acceleration requirements become defined.

STATUS - PER FMC:

See B/700 pg. 19 for logic behind change from two to one elevation cylinder. End-of-stroke cushion is part of the dynamic analysis of elevation and equilibration (C/110).

AUTHOR: Jeff Ireland/Bart Anderson



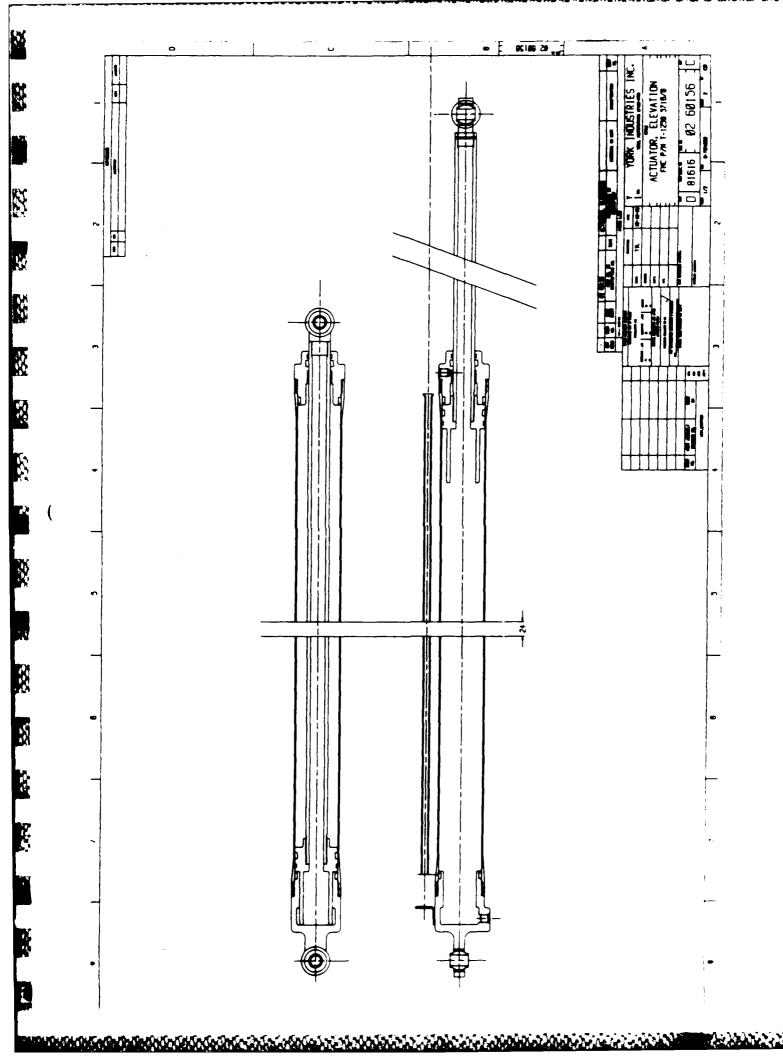
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95109 20 8 YORK INDUSTRIES INC. ACTUATOR, ELEVATION ASSEMBLY FMC PAN THASE S716/8 02 60156 NG28774-138 CYLINGER, WOHINE CYLINGER, TANK FILANDER WAY, REYLAR PISTOR MOHINE PISTOR NO ¥ . 4 91918 ACTUATOR, BLEVATION AND PISTON
R. 6600-181
SSA. RING
VAN RING
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R. 6600-183
R. 6600-1 NO SEA SOLVED RING SOLVED RING SPECIOL NEARING PISTON HOUNT ı 9 7/03 336 69 AVT 62 4/00:7 62 4/00:7 R2 (80) 38-7 PART RS. (9) MEDIT (17) NS. 48. 3000 336 3000 143 61 62 400X·7 36000-X 62 46000-7 36000-1 62 46000-7 12 MENT 7 1 | 1 | i DECKO - CO 6 . 1 . 2 . ----NOTES:

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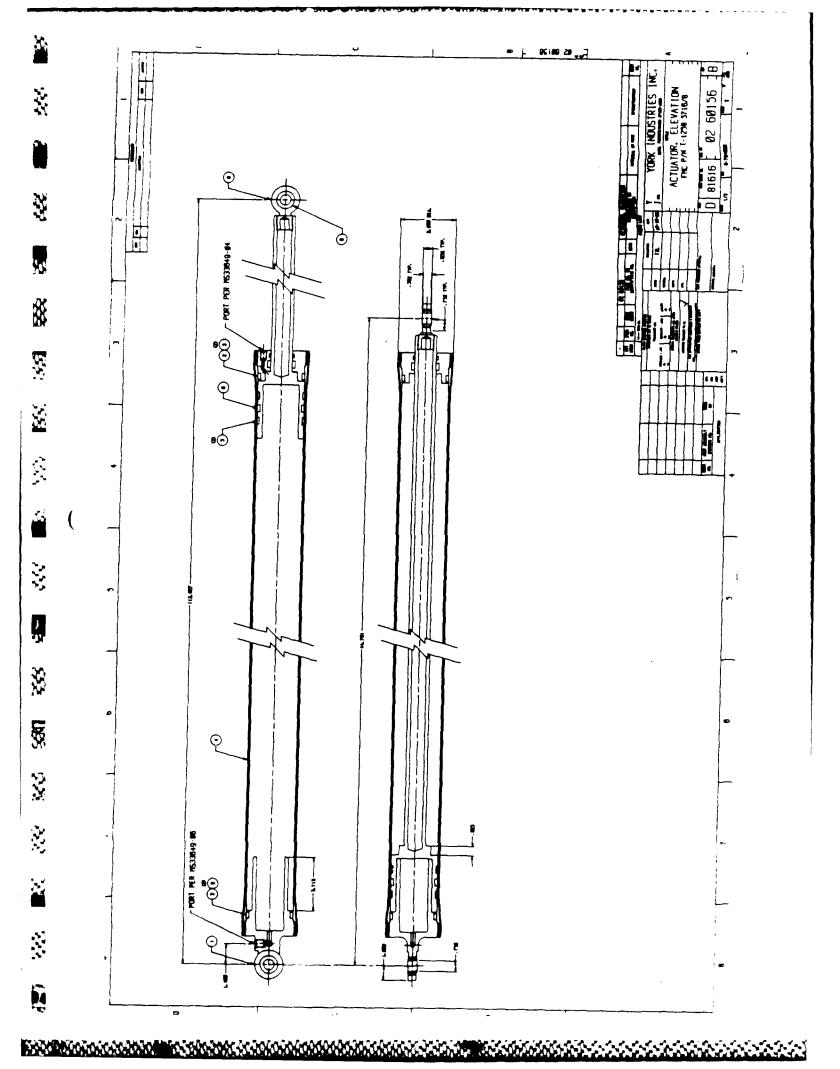
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DESCRIPTION: ELEVATION ACTUATOR (Obsolete)



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C'ALINEER, THE
FILMEDIT WAY, RETAIN
FISSETY-238
FISSETY-238 96109 ACTUATOR, ELEVATION ASSENBLY FMC P/N T-1258 5716/A PISTOR, MONINE PISTOR, MOD ... 81616 ACTUATOR, ELEVATION ABOVE PISTON
RE-4BEXT-7
RE-4BEXT-7
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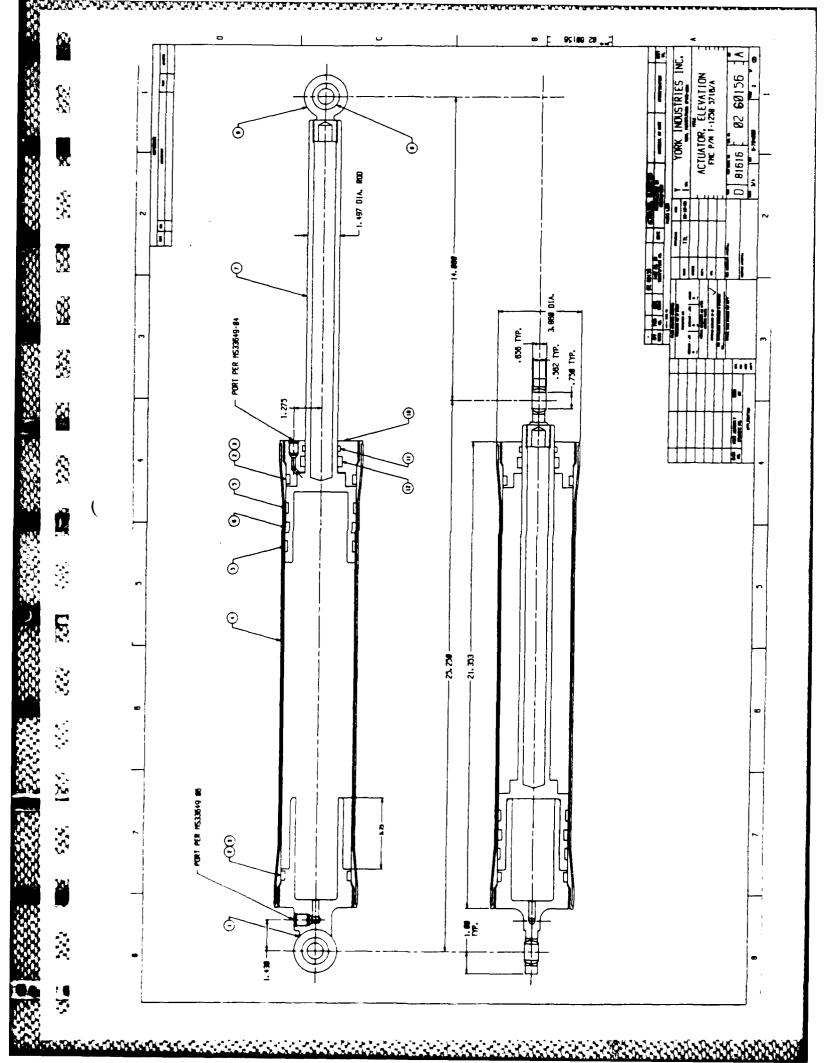
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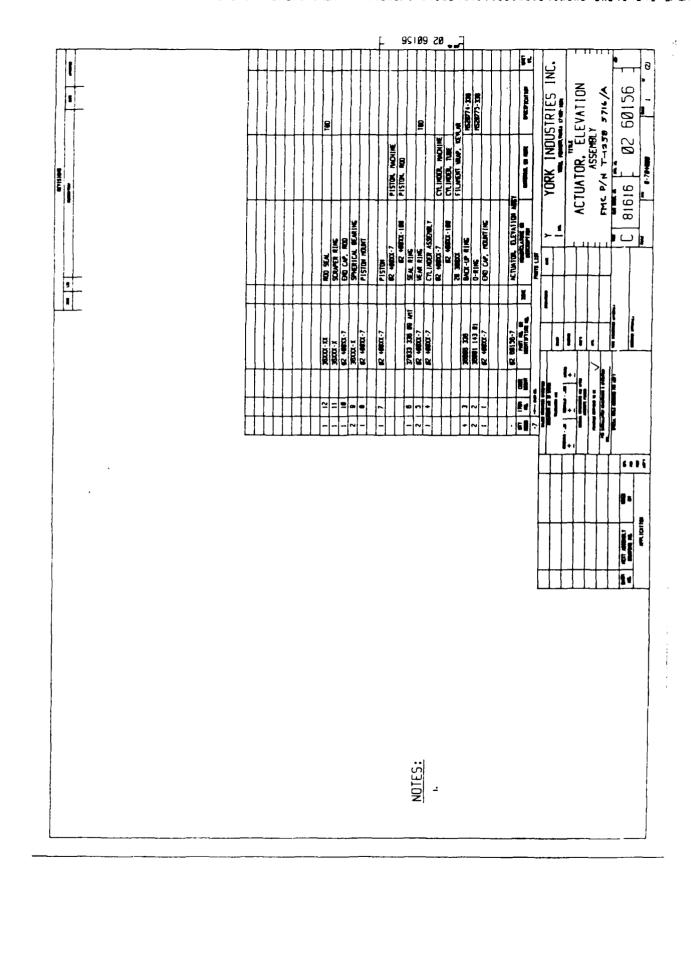
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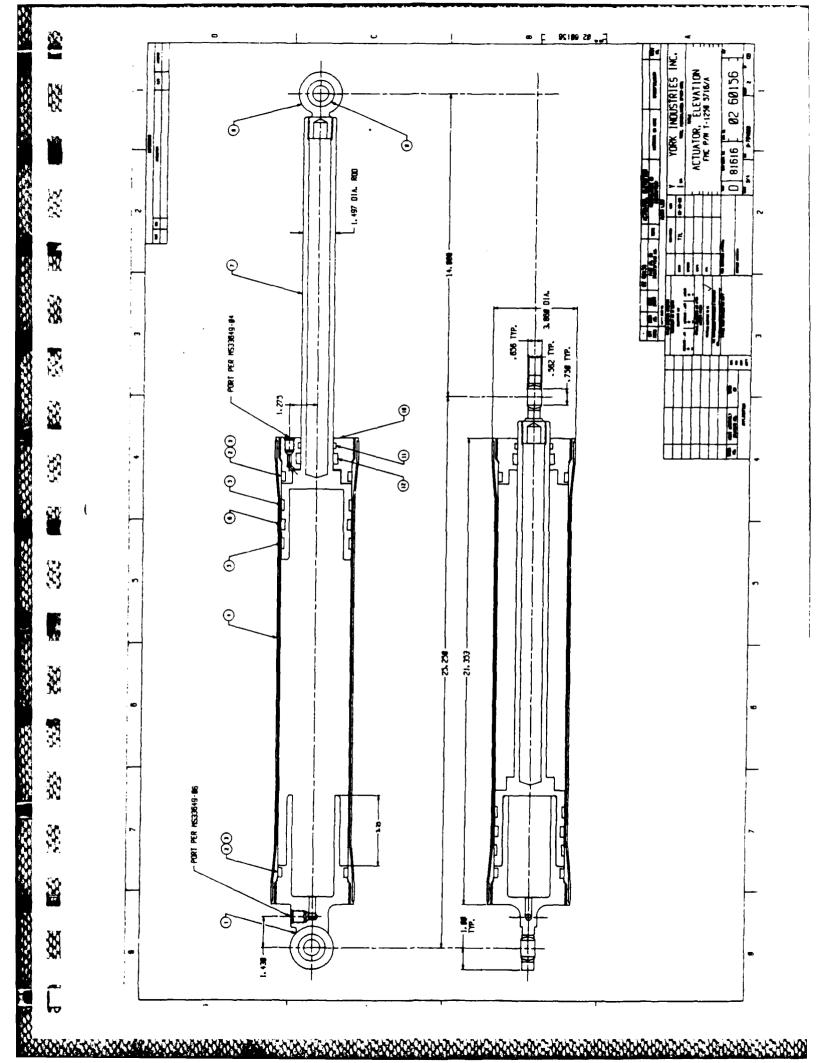
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DESCRIPTION: ELEVATION AND TRAVERSE SYSTEM PERFORMANCE SUMMARY

STATUS - PER YORK:

D322372

An analysis of the static and dynamic performance of the hydraulic systems for elevation and traverse was planned for this program, but was suspended midway through the program so that available resources could be applied to the basis design of the components. Initial results are provided for the early configuration. No effort was expended and, therefore, no results are available which evaluate the fluid inertia effects incurred by operation of the hydraulic subsystems.

STATUS - PER FMC:

Don Sweitzer of York and John Green of FMC conferred on equilibration system analysis. York's analysis efforts tapered off as the FMC model and York model began to provide similar results. See Section C/110 (Elevation and Equilibration), C/240 (Traverse Actuator), and C/260 (Tube Laying Accuracy).

AUTHOR: Jeff Ireland/Bart Anderson

ELEVATION SYSTEM PERFORMANCE SUMMARY		5/10/ 13: 8:	87 29
POLITITEDATION OVITHDED DADAMETERS.			
PISTON DIAMETER ROD DIAMETER RETRACT PRESSURE AREA STROKE NOMINAL OPERATING PRESSURE RETRACT FORCE AT NOMINAL PRESSURE MAXIMUM OPERATING PRESSURE RETRACT FORCE AT MAXIMUM PRESSURE RETRACT FLOWRATE - RATED ELEVATION CYLINDER PARAMETERS:			
PISTON DIAMETER ROD DIAMETER STROKE MINIMUM OPERATING PRESSURE EXTEND FORCE AT MINIMUM PRESSURE RETRACT FORCE AT MINIMUM PRESSURE MAXIMUM OPERATING PRESSURE EXTEND FORCE AT MAXIMUM PRESSURE RETRACT FORCE AT MAXIMUM PRESSURE RETRACT FORCE AT MAXIMUM PRESSURE RETRACT FORCE AT MAXIMUM PRESSURE EXTEND FLOWRATE - RATED RETRACT FLOWRATE - RATED	INCH INCH INCH PSIG LBS LBS PSIG LBS LBS CBS	3.250 1.500 38.567 3000. 24887. 19586. 3200. 26546. 20892. 72.540 92.175	
EQUILIBRATION ACCUMULATOR PARAMETERS:			
ACCUMULATOR VOLUME CHARGE PRESSURE AT 70 deg-F STARTING PRESSURE AT 0 Q.E.	PSIA PSIA	2800.00 5200.00	
SYSTEM CONFIGURATION PARAMETERS:			
PIVOT COORDINATES EQUILIBRATION FIXED MOUNT EQUILIBRATION MOVABLE END O Q.E. ELEVATION CYLINDER FIXED MOUNT ELEVATION CYLINDER MOVABLE END AT O Q.E. CENTER OF GRAVITY COORDINATES ELEVATING WEIGHT MASS MOMENT OF INERTIA	INCH INCH INCH INCH INCH INCH LNCH INCH LBS SLUG-FT^2	0.000 -2.000 242.250 161.750 -10.000 96.000 6077.00 41230.0	0.000 35.500 -8.500 3.100 35.000 18.500

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ISO	0.	72.						160.	160.
ISO	0.	72.						-25.	-25.
ISO	0.	72.		3486.				70.	120.
ISO	0.	72.						-25.	25.
ISO	ο.	72.		3848.				70.	50.
ISO	0.	72.	5386.	4152.	1047.	403.		160.	140.
ISO	0.	72.			886.			70.	70.
ISO	0.	72.		4041.		2021.		160.	160.
ISO	0.	72.		3335.	818.	1567.		-25.	-25.
ISO	0.	72.	5200.	3738.	1827.	345.		70.	70.
ISO	Ο.	72.	5200.	4041.		404.		160.	160.
ISO	0.	72.	5200.	3335.		283.		-25.	-25.
ADIA		72.	5200.	3266.	1435.	365.	0.	70.	70.
ADIA		72.	5200.	3596.	1327.	427.	0.	160.	160.
ADIA		72.	5200.	2828.	1621.	300.		-25.	-25.
ADIA		72.	4725.	3085.	1671.	365.	0.	70.	120.
ADIA		72.	4637.	2677.	1836.	300.	0.	-25.	25.
ADIA		72.	5416.	3344.	1344.	365.	0.	70.	50.
ADIA		72.	5386.	3680.	1229.	427.	0.	160.	140.
ADIA		72.	5200.	3266.	886.	1597.	18.	70.	70.
ADIA	0.	72.	5200.	3596.	951.	1813.	18.	160.	160.
ADIA		72.	5200.	2828.	865.	1322.	18.	-25.	-25.
ADIA		72.	5200.	3266.	2158.	365.	-10.	70.	70.
ADIA	0.	72.	5200.	3596.	2023.	427.	-10.	160.	160.
ADIA	0.	72.	5200.	2828.	2359.	300.	-10.	-25.	-25.
ADIA	72.	0.		4033.	301.	1621.	0.	70.	70.
ADIA	72.	0.	5827.	4177.	352.	1381.	0.	160.	160.
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ADIA	72.	0.	6052.	4296.	352.	1538.	0.	160.	140.
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MAXIMI ENERGY ENERGY PISTOI	ING DECEL UM DECELE Y STORE A Y STORE A N DIAMETE IAMETER	RATION : CCUM GAS CCUM PRI	TORQUE S VOLUME		PSIA FT-LB IN-3 PSIA INCH INCH	100 24 30	000.000	
SYSTE	M PARAMET	ERS:						
ENDING ELEVA:	ING ELEVATIFING WEIG	ON (TI	HETAf)		DEGREE LBS	S	72.000 77.000	
TIME	ANGLE	PRESS	PRESS	PRESS	ANGULAR VELOCITY	PLOW	PLOW	
SEC	DEGREE	PSIA	PSIA	PSIA	DEG/SEC	GPM	GPM	
0.100 0.200 0.300 0.400 0.500	0.000 0.231 0.892 1.903 3.168 4.596 6.119 7.690 9.279 10.869 12.450 14.019 15.573 17.113 18.638 20.150 21.650 23.140	356.1 497.8 668.9 821.2 933.6	2944.6 2803.4 2633.1 2481.7 2370.5	5190.3 5162.3 5119.8 5067.0 5008.1	0.023 4.548 8.508 11.535 13.594 14.850 15.530 15.835 15.916 15.869 15.758 15.617 15.468 15.321 15.185 15.060 14.950 14.854	5.634 10.615 14.502 17.236 18.995	4.434 8.354 11.413 13.564 14.949 15.771 16.216 16.426 16.496 16.487 16.435 16.363 16.281 16.198 16.118	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

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TIME	ANGLE	EXTEND	RETRACT	EQUIL	ANGULAR	EXTEND	RETRAC	T
		PRESS	PRESS		VELOCITY			1
SEC	DEGREE					FLOW	FLOW	
320	DEGREE	PSIA	PSIA	PSIA	DEG/SEC	GPM	GPM	
1 000	0/ /00							
1.800	24.622	1034.0	2287.6	4269.6	14.772	20.207	15.903	1
1.900	26.095	1030.0	2293.1	4222.3	14.706	20.130	15.842	1
2.000	27.563	1026.5	2298.0	4176.3		20.060	15.787	ī
2.100	29.027	1023.5	2302.4	4131.4		19.996	15.737	i
2.200	30.487	1020.9	2306.4	4087.6	14.595	19.939		
2.300	31.946	1018.8	2309.9	4044.9			15.692	1
2.400	33.405	1017.1				19.889	15.652	1
2.500			2313.0	4003.2	14.594	19.844	15.617	1
	34.865	1015.9	2315.7	3962.5	14.617	19.805	15.586	1
2.600	36.329	1015.0	2318.0	3922.7	14.655	19.771	15.559	1
2.700	37,797	1014.4	2320.0	3883.8	14.709	19.742	15.537	1
2.800	39,271	1014.2	2321.7	3845.8	14.780	19.718	15.518	i
2.900	40.754	1014.3	2323.1	3808.7	14.869	19.698	15.502	
3.000	42,246	1014.6	2324.2	3772.4				1
3.100	43.750	1015.2	2325.2		14.976	19.681	15.489	1
3.200	45.267			3736.8	15.103	19.667	15.478	1
		1015.9	2325.9	3702.1	15.252	19.656	15.469	1
3.300	46.801	1016.8	2326.6	3668.1	15.424	19.647	15.462	1
3.400	48.353	1017.7	2327.2	3634.8	15.622	19.638	15.455	1
3.500	49.926	1018.6	2327.8	3602.2	15.847	19.629	15.448	1
3.600	51.523	1019.4	2328.6	3570.4	16.103	19.618	15.439	ì
3.700	53,148	1020.0	2329.6	3539.2	16.393	19.604	15.428	i
3.800	54.804	1020.1	2331.0	3508.7	16.722	19.583		,
3.900	56.481	1421.6	1931.1	3479.1	16.345		15.411	1
4.000	58.032	1406.3	1947.8			18.711	14.725	3 3
4.100	59.431			3452.9	14.727	16.464	12.957	3
		1392.4	1962.9	3430.2	13.270	14.494	11.407	3
4.200	60.691	1379.9	1976.6	3410.5	11.957	12.769	10.049	3
4.300	61.826	1368.4	1989.0	3393.4	10.774	11.258	8.860	3
4.400	62.849	1358.0	2000.3	3378.5	9.708	9.935	7.819	3
4.500	63.770	1348.4	2010.7	3365.5	8.747	8.776	6.907	3
4.600	64.601	1339.6	2020.2	3354.1	7.882	7.761	6.108	3
4.700	65.349	1331.5	2028.9	3344.2	7.102	6.871	5.407	2
4.800	66.023	1324.1	2036.9	3335.4				3
4.900	66.631	1317.2			6.399	6.089	4.792	3
5.000			2044.2	3327.6	5.766	5.403	4.252	3
	67.178	1310.9	2050.9	3320.8	5.195	4.799	3.776	3
5.100	67.672	1305.1	2057.1	3314.8	4.681	4.266	3.357	3
5.200	68.116	1299.8	2062.7	3309.4	4.218	3.797	2.988	3
5.300	68.516	1295.0	2067.9	3304.7	3.801	3.382	2.662	3
5.400	68.877	1290.5	2072.7	3300.5	3.424	3.016	2.373	3
5.500	69.202	1286.4	2077.0	3296.7	3.086	2.691	2.118	
5.600	69.495	1282.7	2081.0	3293.4				3
5.700	69.759	1279.2			2.780	2.403	1.891	3
5.800			2084.6	3290.4	2.505	2.148	1.691	3
	69.997	1276.1	2087.9	3287.8	2.257	1.921	1.512	3
5.900	70.211	1273.3	2090.9	3285.4	2.034	1.719	1.353	3
6.000	70.405	1270.7	2093.6	3283.3	1.833	1.540	1.212	3
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DYNAMIC ANALYSIS	5/10/87
ENERGY RECOVERY ELEVATION - Adiabatic	

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ENEKGI	KECOVER	Y ELEVAT	TION - Ad	iabatic				
TIME	ANGLE	EXTEND	RETRACT	EQUIL	ANGULAR	EXTEND	RETRACT	
		PRESS	PRESS	PRESS	VELOCITY	FLOW	FLOW	
SEC	DEGREE	PSIA	PSIA	PSIA	DEG/SEC	GPM	GPM	
6.100	70.579	1268.3	2096.1	3281.4		1.380	1.086	3
6.200	70.735	1266.2	2098.3	3279.7	1.488	1.237	0.973	3
6.300	70.877	1264.2	2100.4	3278.2	1.341	1.109	0.873	3
6.400	71.004	1262.4	2102.3	3276.8	1.208	0.995	0.783	3
6.500	71.119	1260.8	2103.9	3275.6	1.088	0.893	0.703	3
6.600	71.222	1259.4	2105.5	3274.5	0.981	0.802	0.631	3
6.700	71.315	1258.0	2106.9	3273.6	0.884	0.720	0.567	3
6.800	71.399	1256.8	2108.1	3272.7	0.796	0.647	0.509	3
6.900	71.475	1255.8	2109.3	3271.9	0.717	0.582	0.458	3 3 3 3 3 3 3
7.000	71.543	1254.8	2110.3	3271.2	0.646	0.523	0.412	3
7.100	71.604	1253.9	2111.2	3270.5	0.583	0.470	0.370	3
7.200	71.659	1253.1	2112.1	3270.0	0.525	0.423	0.333	3 3 3
7.300	71.709	1252.4	2112.8	3269.5	0.473	0.380	0.299	3
7.400	71.754	1251.7	2113.5	3269.0	0.426	0.342	0.269	3
7.500	71.795	1251.1	2114.1	3268.6	0.384	0.308	0.242	3 3
7.600	71.831	1250.6	2114.7	3268.2	0.346	0.277	0.218	
7.700	71.864	1250.1	2115.2	3267.9	0.312	0.249	0.196	3
7.800	71.893	1249.6	2115.7	3267.6	0.281	0.224	0.177	3
7.900	71.920	1249.3	2116.1	3267.3	0.253	0.202	0.159	3 3
8.000	71.944	1248.9	2116.4	3267.0	0.228	0.182	0.143	3
8.100	71.966	1248.6	2116.8	3266.8	0.205	0.164	0.129	3
8.200	71.985	1248.3	2117.1	3266.6	0.185	0.147	0.116	3
8.300	72.000	1243.2	2122.2	3266.5		0.000	0.000	3

ENERGY		Y ELEVA	TION - Ad				5/10/87 13:15:58
PISTON EQUILI AMBIEN CHARGE	N AREA (2 BRATION NT TEMPER PRESSUR	ACCUMUL	R PARAMET ATOR VOLU deg-F O Q.E. FROM 70	IME	IN^2 IN^3 deg-F PSIA PSIA IN^3	1 2 5	5.522 200.00 160.00 800.00 200.00 -99.39
ELEVAT	TION CYLI	NDER PA	RAMETERS:				
ENERGY PISTON	ING DECEL JM DECELE (STORE A (STORE A N DIAMETE LAMETER	CCUM PR	PRESSURE TORQUE S VOLUME ESSURE	;	PSIA FT-LB IN 3 PSIA INCH INCH	30 100 24 30	000.000 000.000 000.000 000.000 3.250 1.500
SYSTEM	1 PARAMET	ERS:					
ENDING ELEVAT	G BLBVATI Ting wrig	ON (T) HT	HETAO) HETAf)		DEGREE DEGREE LBS Slug-F	S	72.000
		EXTEND	RETRACT PRESS	EQUIL			
SEC	DEGREE		PSIA				
0.400 0.500	3.080 4.481 5.982	850.0 963.6 1040.0	2317.1	5100.2 5055.3 5007.5	13.302 14.604 15.345	16.856 18.668 19.785	13.266 1 14.691 1

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	TO BECOUR						5/10/	87
ENEK(GY RECOVE	RY ELEVA	TION - A	diabatic				
TIME	ANGLE	EXTEND	RETRACT	EQUIL	ANGULAR	EXTEND	RETRAC	T
		PRESS	PRESS		VELOCITY			
SEC	DEGREE	PSIA				FLOW	FLOW	
320	DEGREE	PSIA	PSIA	PSIA	DEG/SEC	GPM	GPM	
1 900	24 405							
1.800	24.625	1121.6	2254.7		15.110	20.669	16.266	1
1.900	26.134	1120.4	2257.6	4419.6	15.071	20.629	16.235	
2.000	27.640	1119.5	2260.1	4380.4		20.594	16.207	
2.100	29.144	1119.0	2262.4	4342.1	15.032	20.562		
2.200	30.647	1118.7	2264.3	4304.5			16.182	
2.300	32.151	1118.8	2266.0	4267.6		20.535	16.161	1
2.400	33.657	1119.1				20,512	16.143	1
2.500	35.167		2267.4	4231.5		20.493	16.127	1
2.600		1119.7	2268.5	4196.1	15.125	20.477	16.115	1
	36.683	1120.6	2269.4	4161.3	15.186	20.464	16.105	1
2.700	38.205	1121.6	2270.1	4127.3	15.264	20,454	16.097	1
2.800	39.736	1122.9	2270.6	4093.8		20.447	16.091	1
2.900	41.278	1124.3	2271.0	4061.1		20.442	16.087	
3.000	42.831	1125.9	2271.2	4028.9	15.606			1
3.100	44.400	1127.5	2271.4	3997.4		20.438	16.085	1
3.200	45.985	1129.2			15.761	20.436	16.083	1
3.300	47.589		2271.6	3966.4	15.940	20.433	16.081	1
		1130.8	2271.8	3936.1	16.144	20.430	16.078	1
3.400	49.214	1132.3	2272.1	3906.3	16.377	20.426	16.075	1
3.500	50.865	1133.6	2272.7	3877.1	16.641	20.418	16.068	1
3.600	52.544	1134.5	2273.7	3848.5	16.941	20.404	16.058	ĵ
3.700	54.255	1135.0	2275.2	3820.4	17.281	20.383	16.041	,
3.800	55.987	1546.6	1865.4	3793.2	16.859	19.438		1
3.900	57.588	1531.1	1882.7	3769.0			15.297	3
4.000	59.030	1517.1			15.191	17.102	13.459	3
4.100	60.329		1898.2	3748.0	13.688	15.053	11.847	3
4.200		1504.3	1912.3	3729.9	12.333	13.258	10.434	3
	61.500	1492.7	1925.1	3714.1	11.113	11.687	9.197	3
4.300	62.555	1482.1	1936.8	3700.3	10.013	10.310	8.114	3
4.400	63.506	1472.3	1947.5	3688.2	9.023	9.105	7.166	3
4.500	64.363	1463.3	1957.3	3677.7	8.130	8.049	6.335	3
4.600	65.135	1455.1	1966.3	3668.4	7.325			
4.700	65.830	1447.5	1974.6	3660.3		7.124	5.606	3
4.800	66.457	1440.5	1982.2		6.600	6.311	4.967	3
4.900	67.021			3653.1	5.947	5.598	4.405	3
		1434.0	1989.1	3646.8	5.359	4.970	3.912	3
5.000	67.530	1428.1	1995.5	3641.2	4.829	4.418	3.477	3
5.100	67.989	1422.7	2001.4	3636.2	4.351	3.930	3.093	3
5.200	68.402	1417.7	2006.7	3631.8		3.500	2.755	3
5.300	68.774	1413.1	2011.6	3627.9	3.532	3.120	2.456	
5.400	69.109	1408.9	2016.1	3624.4	3.183	2.784		3
5.500	69.411	1405.0	2020.2	3621.3			2.191	3
5.600	69.684	1401.5	2024.0		2.868	2.485	1.956	3
5.700	69.929			3618.6	2.584	2.221	1.748	3
5.800		1398.3	2027.4	3616.1	2.328	1.986	1.563	3
	70.150	1395.4	2030.5	3613.9	2.098	1.777	1.398	3
5.900	70.349	1392.7	2033.4	3612.0	1.890	1.591	1.252	3
6.000	70.529	1390.3	2035.9	3610.2	1.703	1.425	1.122	3
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	IC ANALYS Y RECOVER		TION - Ad	liabatic			5/10/87 13:15:58
EQUIL	IBRATION	CYLINDE	R PARAMET	ERS:			
EQUIL AMBIE CHARG	N AREA (2 IBRATION NT TEMPER E PRESSUR ING PRESS OLUME ADJ	ACCUMULA ATURE E AT 70	des-F	ME deg-F	IN ² IN ³ deg-F PSIA PSIA IN ³	1 2 5	5.522 200.00 -25.00 800.00 200.00 102.15
ELEVA	TION CYLI	NDER PAI	RAMETERS:	_			
MAXIM ENERG ENERG PISTO	ING DECEL UM DECELE Y STORE A Y STORE A N DIAMETE IAMETER	RATION T CCUM GAS CCUM PRI	TORQUE S VOLUME		FT-LB IN ³	30 100 24 30	000.000
SYSTE	M PARAMET	ERS:					
RTEAV	ING BLEVA G ELBVATI TING WEIG MOMBNT OF	HT			LBS	S S 60 T^2 412	177 .00 0
	ANGLE	PRESS	PRESS	PRESS	VELOCITY	PLOW	FLOW
SEC	DEGREE	PSIA	PSIA	PSIA	DEG/SEC	GPM	GPM
0.400 0.500	0.000 0.240 0.922 1.962 3.256 4.707 6.246 7.824 9.411 10.992 12.557 14.102 15.627 17.131 18.616 20.083 21.533 22.969	788.2 896.9 962.6	2460.6 2352.8 2288.1	5016.2 4936.6 4853.8	13.861 15.048 15.643	17.584 19.261 20.200	13.838 1 15.158 1

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	IC ANALYS						5/10/8	3 7
ENERG	Y RECOVE	RY ELEVAT	TION - Ac	liabatic			2,00,0	•
TIME	ANGLE	EXTEND	RETRACT	EQUIL	ANGULAR	EXTEND	RETRACT	r
		PRESS	PRESS		VELOCITY	FLOW	PLOW	
SEC	DEGREE	PSIA	PSIA	PSIA	DEG/SEC	GPM	GPM	
					DE 075E0	0	0.71	
1.800	24.392	919.3	2344.5	4009.3	14.172	19.383	15.254	1
1.900	25.804	911.8	2353.1	3953.7	14.069			1
2.000	27.206	905.1	2360.9			19.256	15.154	1
2.100	28.601	899.2	2368.0	3899.9	13.981	19.140	15.063	1
2.200	29.989			3847.8	13.910	19.034	14.979	1
2.300		893.9	2374.3	3797.2	13.854	18.937	14.903	1
	31.372	889.3	2380.1	3748.2	13.813	18.951	14.835	1
2.400	32.752	885.3	2385.2	3700.6	13.788	18.773	14.774	1
2.500	34.130	881.8	2389.7	3654.4	13.778	18.703	14.719	1
2.600	35.508	879.0	2393.7	3609.4	13.783	18.642	14.671	1
2.700	36.887	876.6	2397.2	3565.7	13.804	18.589	14.629	l
2.800	38.269	874.7	2400.2	3523.0	13.840	18.542	14.592	ì
2.9 00	39.656	873.3	2402.7	3481.7	13.893	18.503	14.561	1
3.000	41.049	872.3	2404.9	3441.3	13.963	18.469	14.535	ì
3.100	42.449	871.6	2406.7	3401.8	14.049	18.442	14.513	
3.200	43.859	871.3	2408.1	3363.2	14.155	18.419		1
3.300	45.281	871.3	2409.3	3325.5	14.279		14.495	1
3.400	46.716	871.5	2410.2			18.401	14.481	1
3.500	48.166			3288.7	14.425	18.386	14.470	1
3.600	49.635	871.9	2411.0	3252.6	14.592	18.375	14.460	1
3.700		872.5	2411.6	3217.4	14.784	18.365	14.453	1
	51.124	873.1	2412.2	3182.9	15.002	18.356	14.446	1
3.800	52.637	873.7	2412.8	3149.1	15.249	18.347	14.438	1
3.900	54.175	874.2	2413.5	3116.1	15.529	18.335	14.429	1
4.000	55.744	874.3	2414.6	3083.9	15.845	18.319	14.417	1
4.100	57. 3 32	1259.7	2030.4	3052.6	15.458	17.471	13.749	3
4.200	58.799	1245.0	2046.2	3024.9	13.928	15.377	12.101	3
4.300	60.122	1231.7	2060.4	3000.9	12.550	13.542	10.657	3 3
4.400	61.313	1219.7	2073.3	2980.2	11.308	11.935	9.392	3
4.500	62.387	1208.7	2085.0	2962.1	10.189	10.528	8.285	3
4.600	63.354	1198.7	2095.7	2946.4	9.181	9.295	7.315	3
4.700	64.226	1189.5	2105.5	2932.6	8.272	8.216	6.466	3
4.800	65.011	1181.1	2114.5	2920.6	7.454)
4.900	65.719	1173.4	2122.7			7.270	5.721	3
5 000	66.357	1166.3	2130.2	2910.0	6.716	5.440	5.068	3
5.100	66.931			2900.7	6.052	5.711	4.494	3
		1159.7	2137.1	2892.5	5.453	5.070	3.99 0	3
5.200	67.449	1153.7	2143.4	2885.3	4.913	4.505	3.545	3
5.300	67.915	1148.2	2149.2	2878.9	4.427	4.008	3.154	3
5.400	68.336	1143.2	2154.6	2873.2	3.989	3.568	2.808	3
5.500	68.714	1138.5	2159.4	2868.2	3.594	3.180	2.503	3
5.600	69.056	1134.3	2163.9	2863.7	3.239	2.837	2.233	3
5.700	69.363	1130.4	2168.0	2859.7	2.918	2.533	1.993	3
5.800	69.640	1126.8	2171.7	2856.2	2.629	2.263	1.781	3
5.900	69.890	1123.6	2175.1	2853.0	2.369	2.023	1.592	3
6.000	70.115	1120.6	2178.2	2850.2	2.135	1.810	1.425	3
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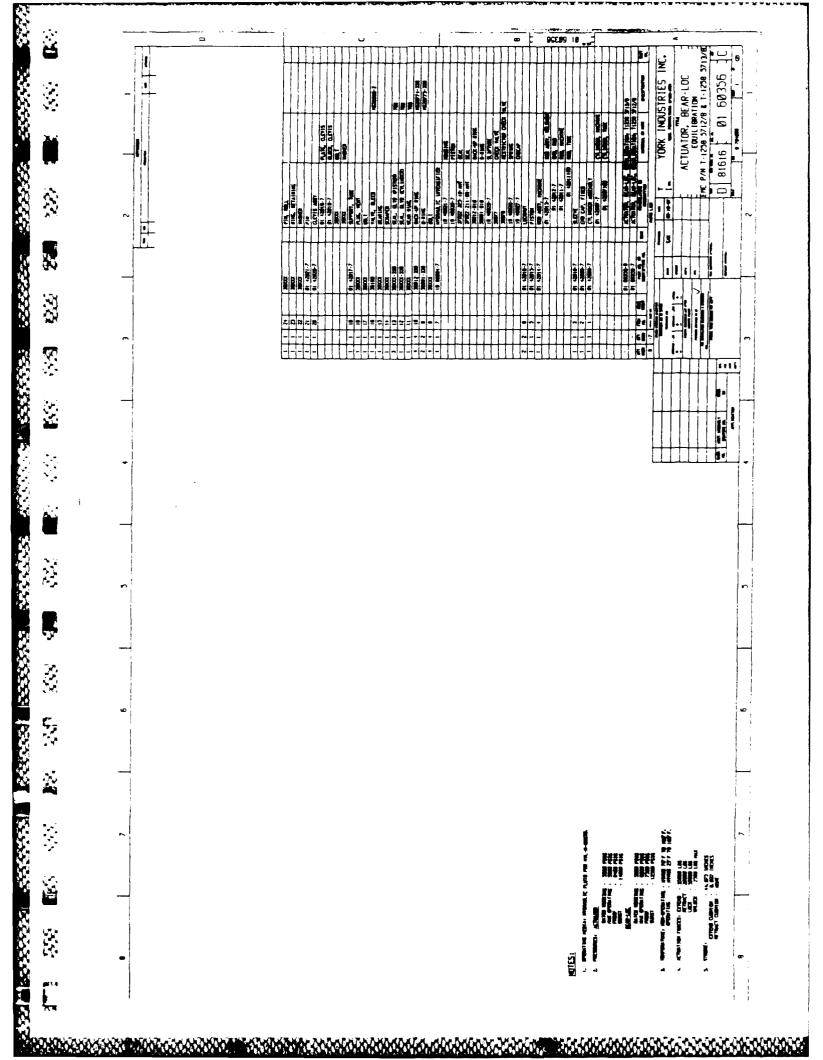
EVENO							3/10/(<i>)</i>
ENERGY	RECOVE		TION - Ad		:			
TIME	ANGLE	EXTEND	RETRACT	EQUIL	ANGULAR	EXTEND	RETRACT	Γ
		PRESS	PRESS	PRESS	VELOCITY	FLOW	FLOW	
SEC	DEGREE	PSIA	PSIA	PSIA	DEG/SEC	GPM	GPM	
6.100	70.317	1117.9	2181.0	2847.7	1 02/	1 (01	1 076	
6.200	70.500	1115.5	2181.6			1.621	1.275	3
6.300	70.665	1113.3		2845.5		1.452	1.142	3
6.400	70.813		2185.9	2843.4		1.301	1.024	3
6.500		1111.2	2188.0	2841.6		1.167	0.918	3
	70.946	1109.3	2189.9	2840.0		1.047	0.824	3
6.600	71.067	1107.7	2191.7	2838.6		0.939	0.739	3
6.700	71.175	1106.1	2193.3	2837.3		0.843	0.664	3
6.800	71.273	1104.8	2194.7	2836.1		0.757	0.596	3
6.900	71.361	1103.5	2196.0	2835.1		0,680	0.535	3
7.000	71.440	1102.4	2197.2	2834.2		0.611	0.481	3
7.100	71.512	1101.4	2198.3	2833.3	0.679	0.549	0.432	3
7.200	71.576	1100.4	2199.2	2832.6	0.611	0.494	0.389	3
7.300	71.634	1099.6	2200.1	2831.9	0.551	0.444	0.350	3
7.400	71.687	1098.8	2200.9	2831.3		0.400	0.314	3
7.500	71.734	1098.1	2201.6	2830.7		0.359	0.283	3
7.600	71.776	1097.5	2202.2	2830.2		0.323	0.254	3
7.700	71.815	1097.0	2202.8	2829.8		0.291	0.229	3333333333 3333 3
7.800	71.849	1096.5	2203.3	2829.4		0.262	0.206	3
7.900	71.880	1096.0	2203.8	2829.0		0.236	0.185	3
8.000	71.908	1095.6	2204.2	2828.7		0.212	0.167	3
8.100	71.933	1095.2	2204.6	2828.4		0.191		3
8.200	71.956	1094.9	2205.0	2828.1		0.172	0.150	3
8.300	71.976	1094.6	2205.3	2827.9			0.135	3
8.400	71.995	1094.3	2205.6			0.155	0.122	3
8.500	72.000	1089.4		2827.7		0.139	0.110	3
J. J. J. U.	72.000	1007.4	2210.5	2827.6	0.170	0.000	0 000	2

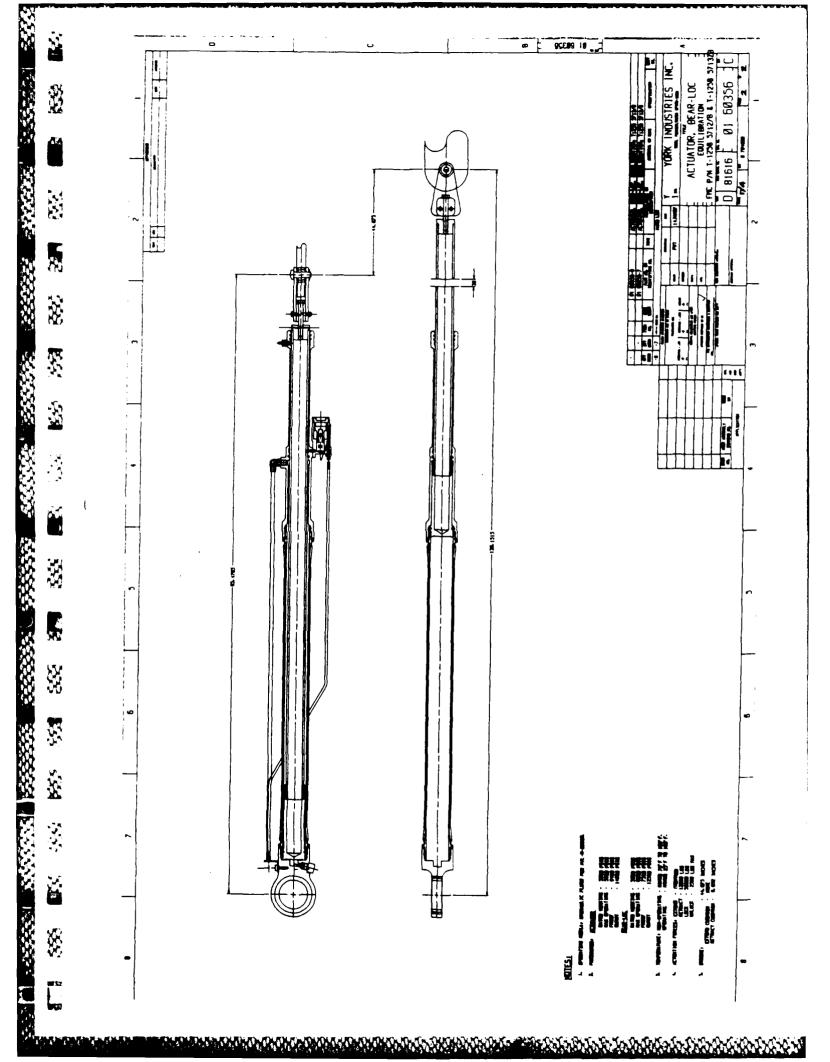
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DESCRIPTION: EQUILIBRATION ACTUATOR - LEFT

STATUS - PER YORK:

The assembly drawing was nearing completion and the stress analysis was begun. This component has been identified by YII as a long lead item and the design was scheduled for fabrication process review and assembly tooling design. This component was well within its weight budget after Kevlar wrapping of the actuator cylinder was incorporated.





DESCRIPTION: EQUILIBRATION ACTUATOR - LEFT (Obsolete)

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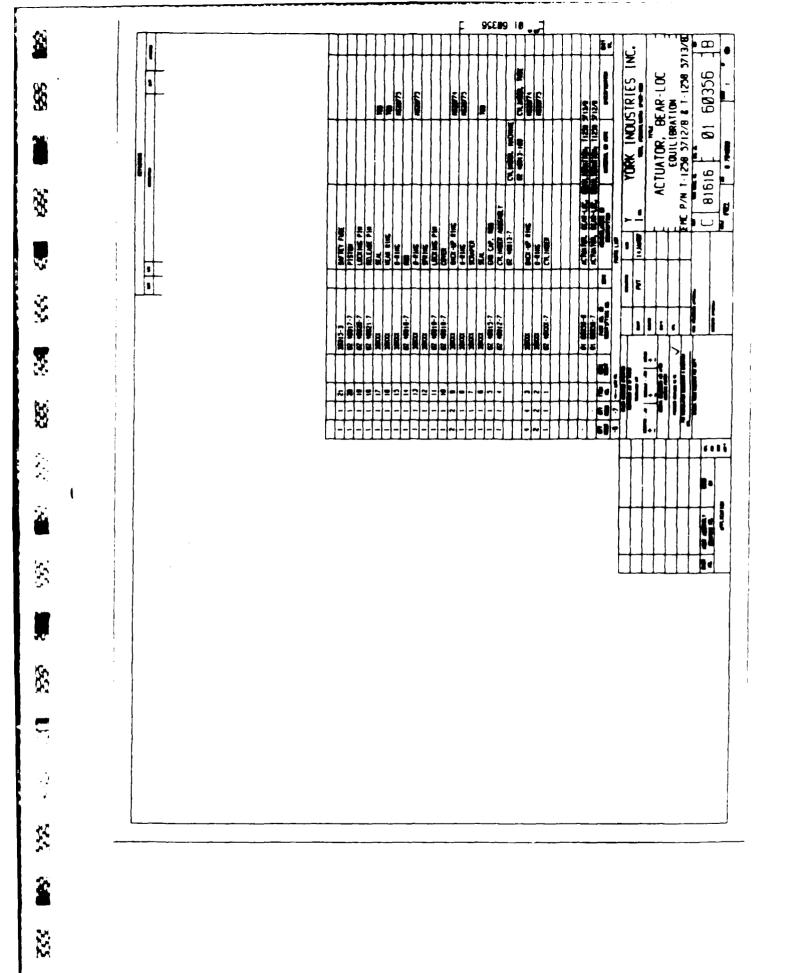
DESCRIPTION: EQUILIBRATION ACTUATOR LEFT (LESOLEI)

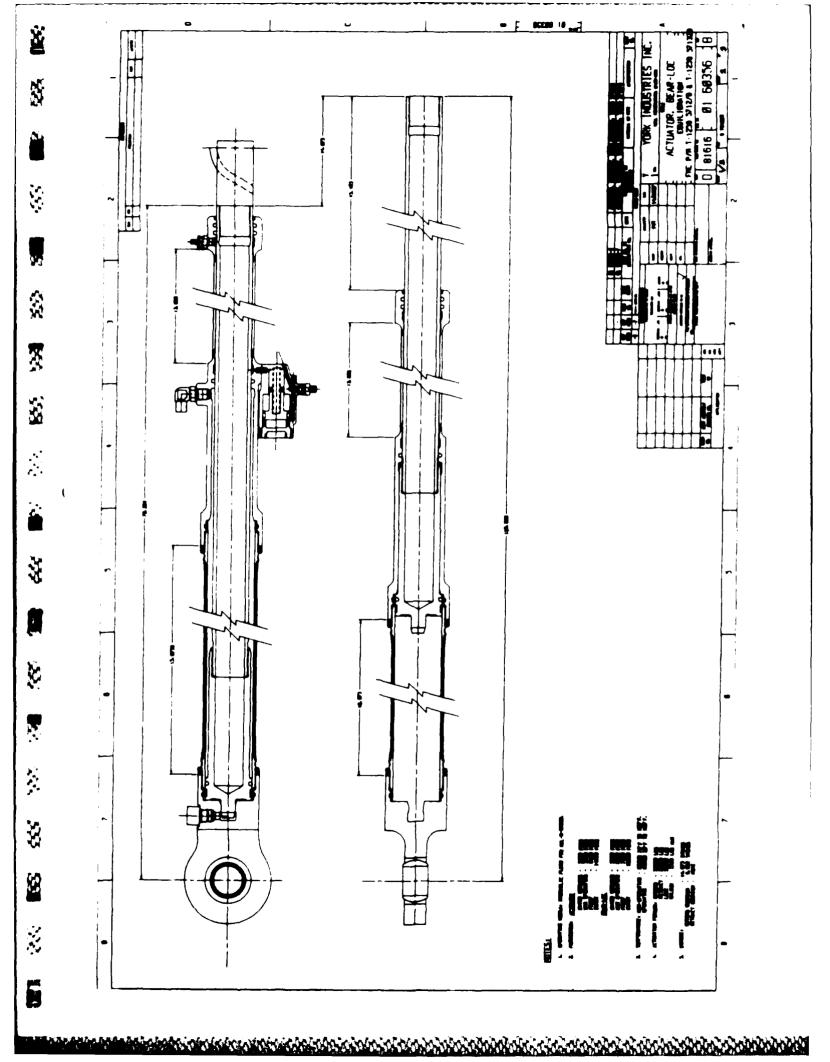
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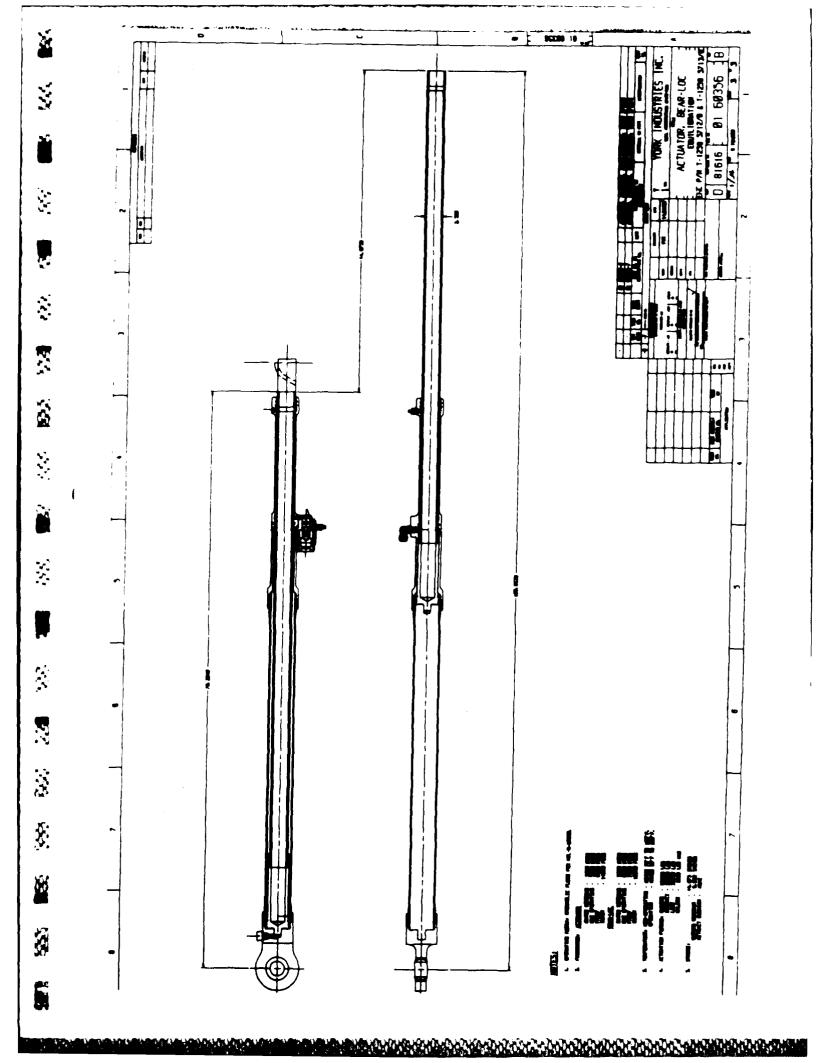
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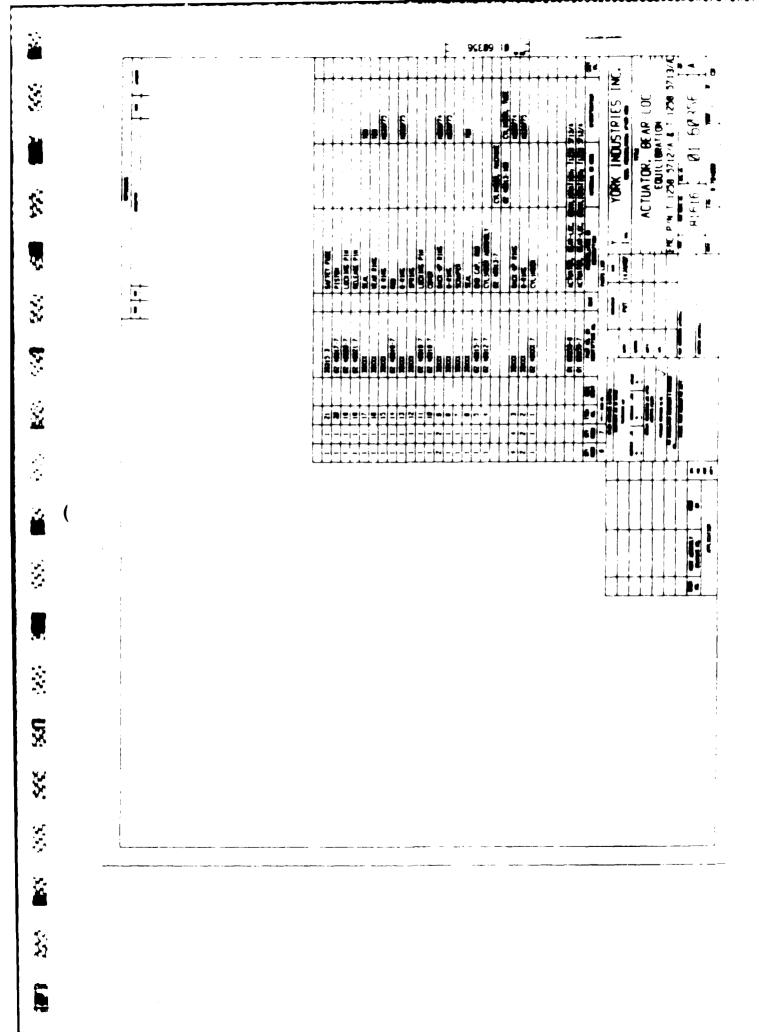
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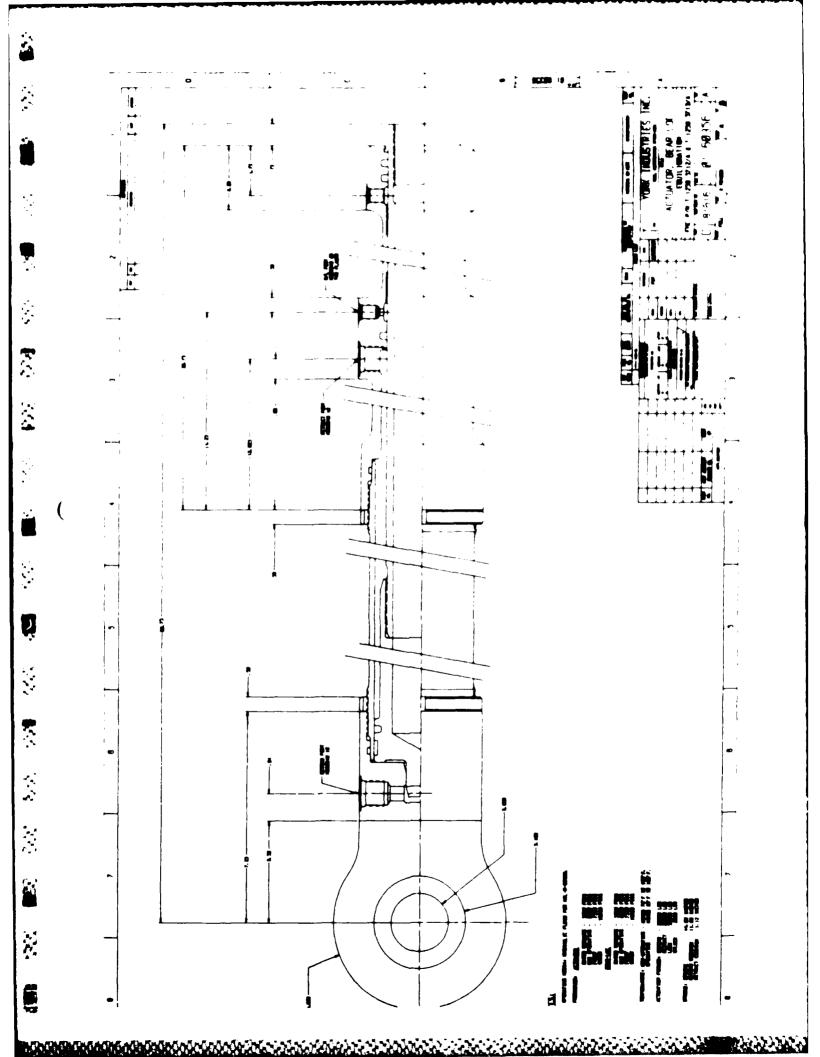
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DESCRIPTION: EQUILIBRATION ACTUATOR - RIGHT

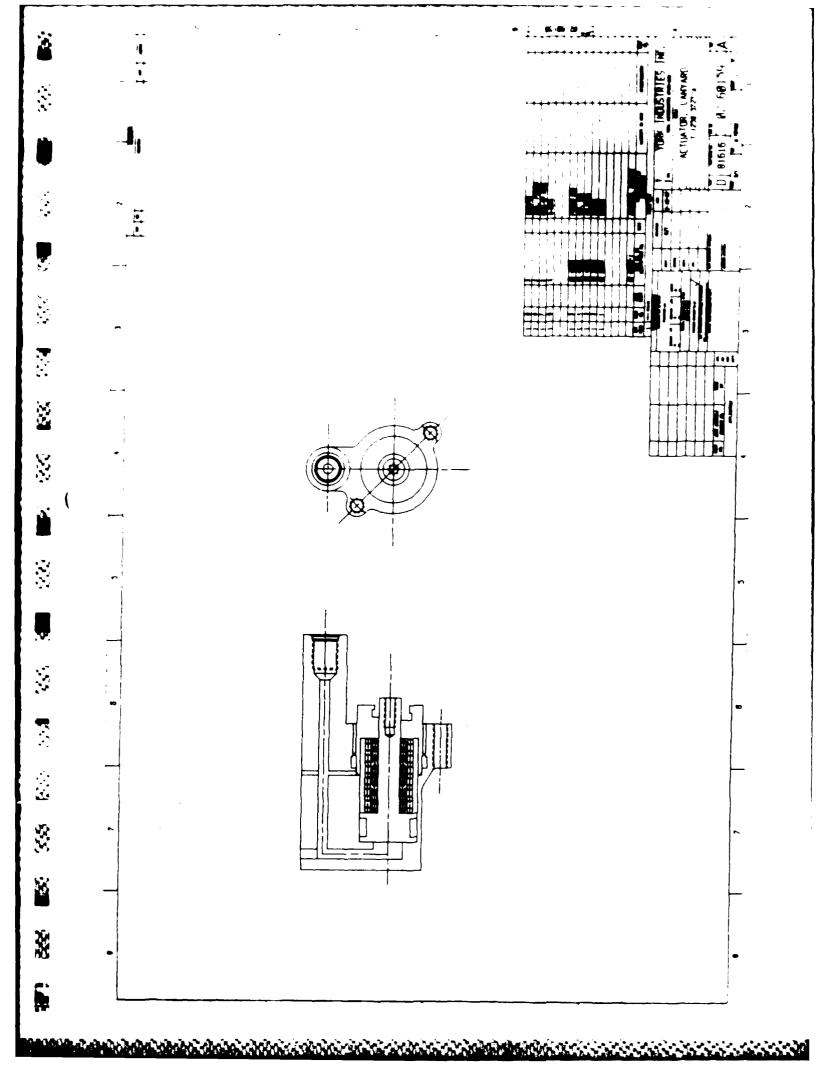
STATUS: See E/190

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DESCRIPTION: LANYARD ACTUATOR

STATUS - PER YORK:

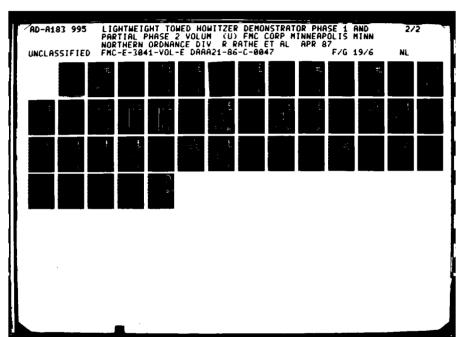
The concept drawing on this actuator was approximately 90% complete. The first review of the design was in progress at the time of contract termination. Although the weight analysis of this actuator had not been updated for the then current design, its estimated weight was near its weight budget and no further weight reduction was anticipated.

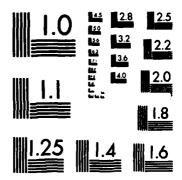


DESCRIPTION: LANYARD ACTUATOR (Obsolete)

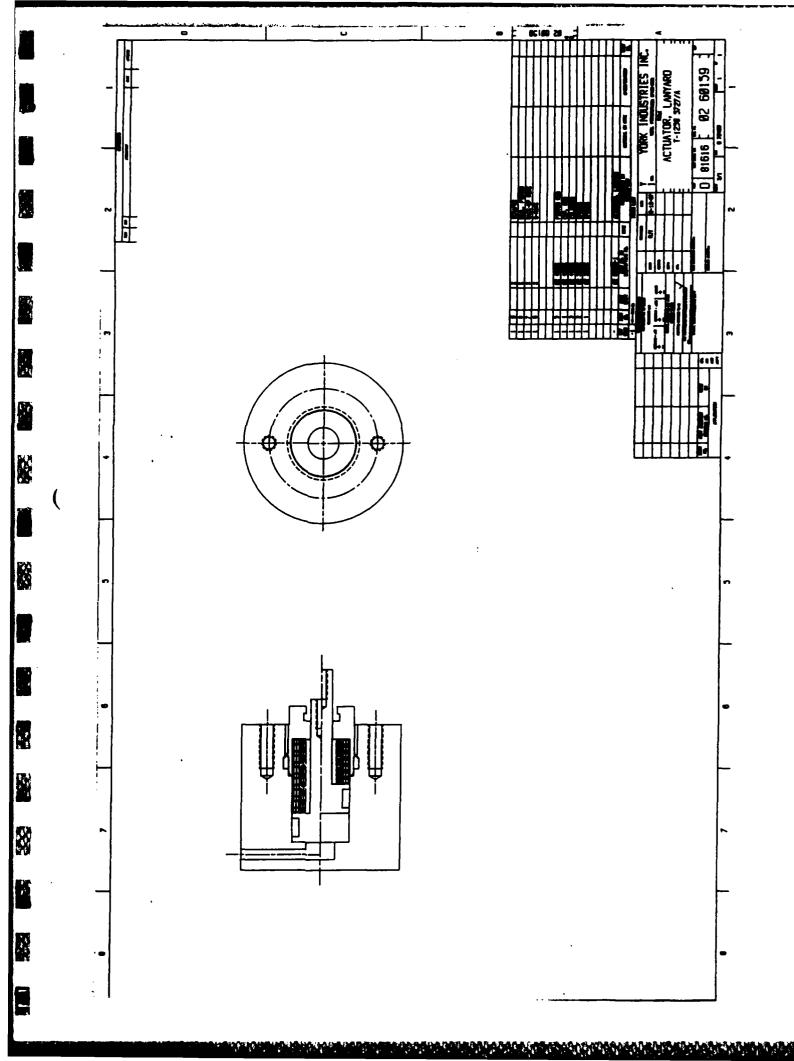
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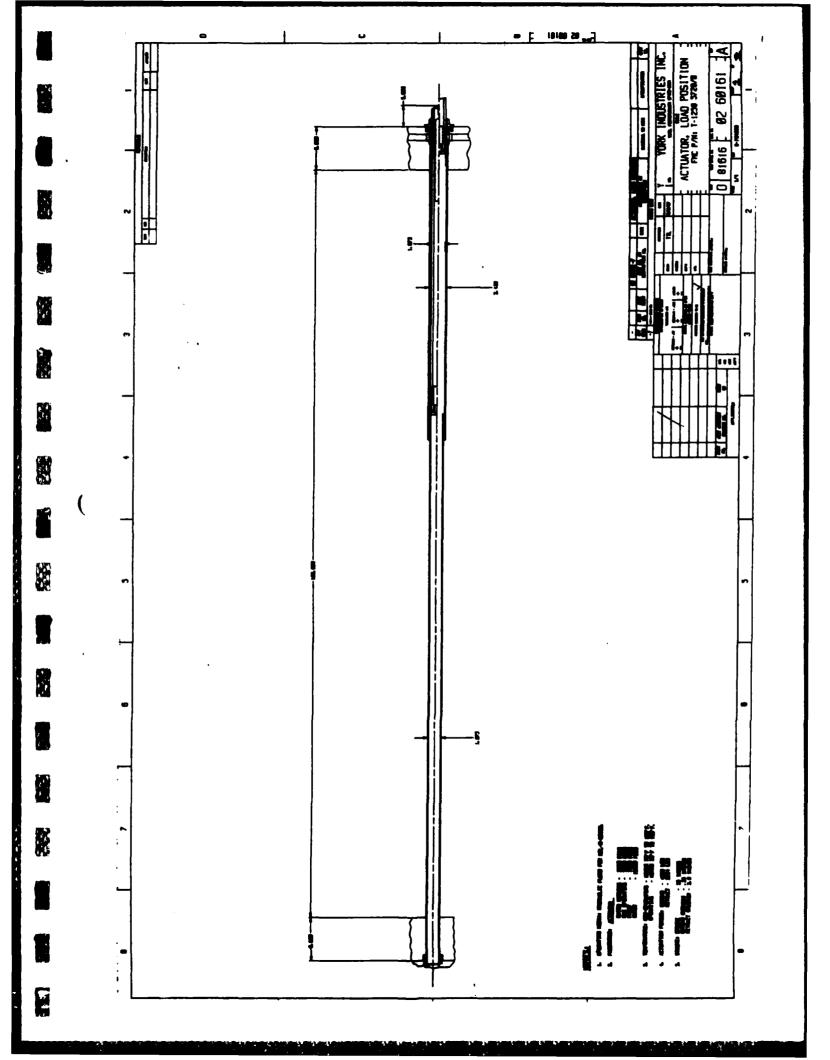


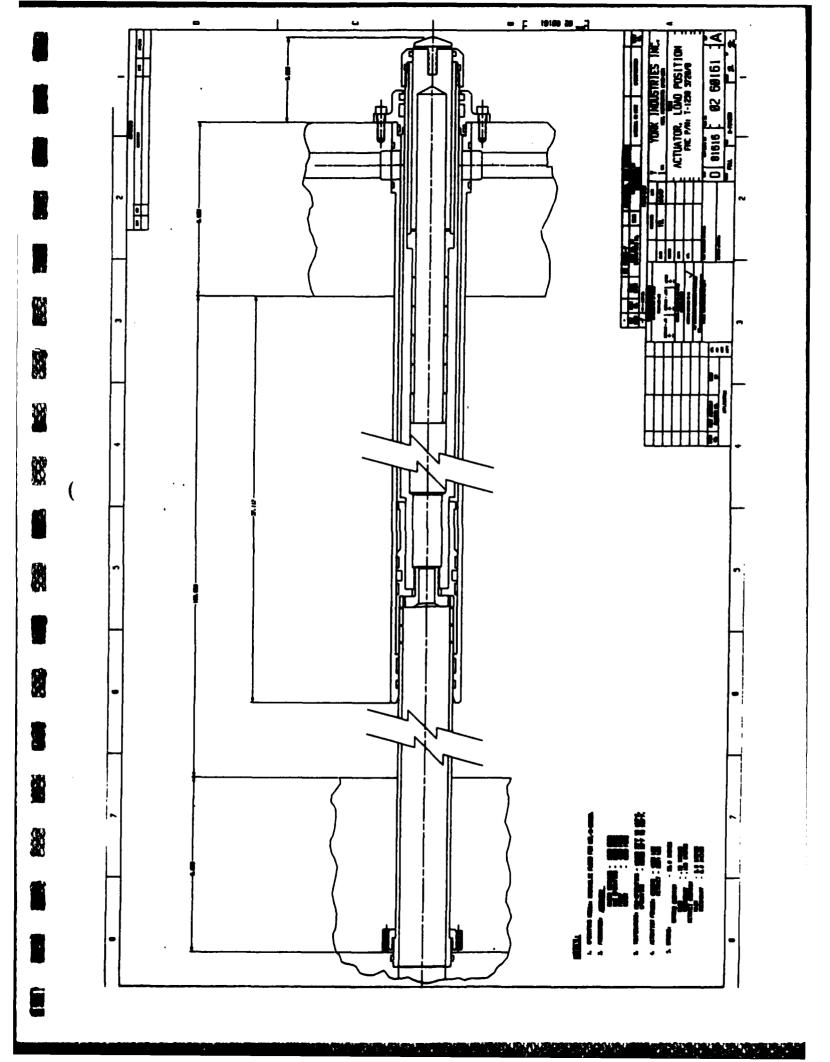
DESCRIPTION: LATCH POSITION ACTUATOR

STATUS - PER YORK:

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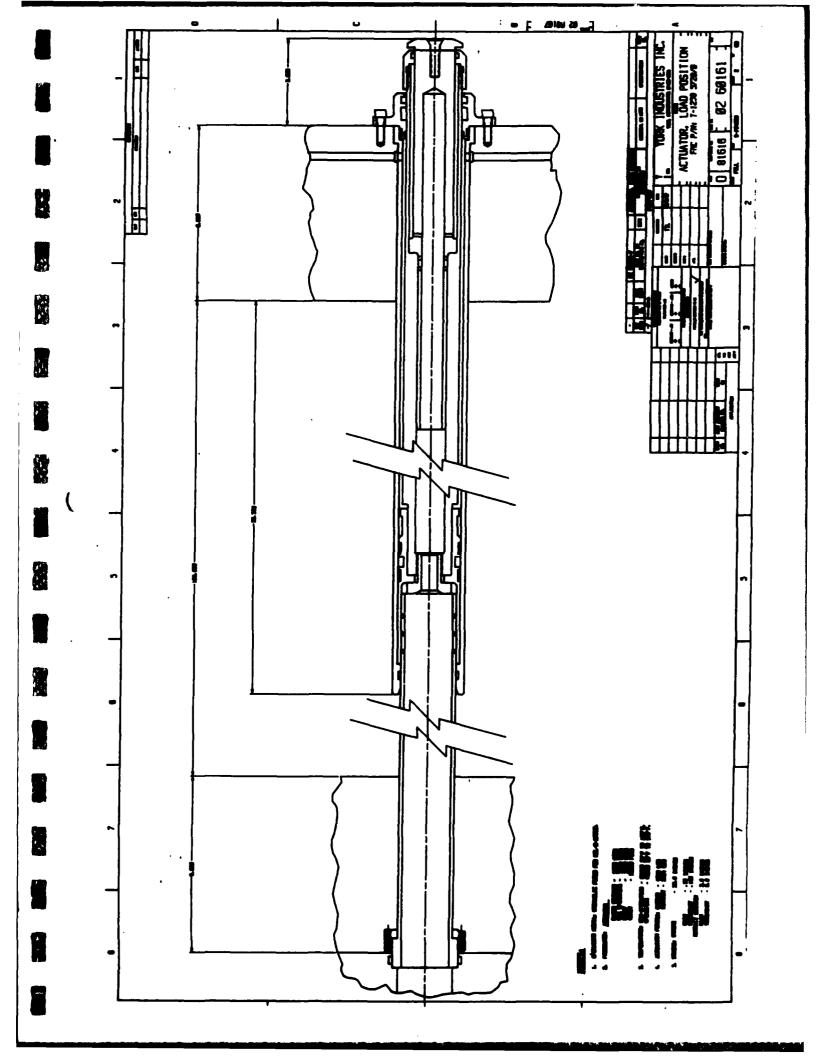
The concept drawing for the load position actuator was complete and the design was in the process of a fabricability review at the time of contract termination. Although the weight analysis of this actuator had not been updated for the then current design, its estimated weight was near its weight budget and no further weight reduction was anticipated.





DESCRIPTION: LATCH POSITION ACTUATOR (Obsolete)

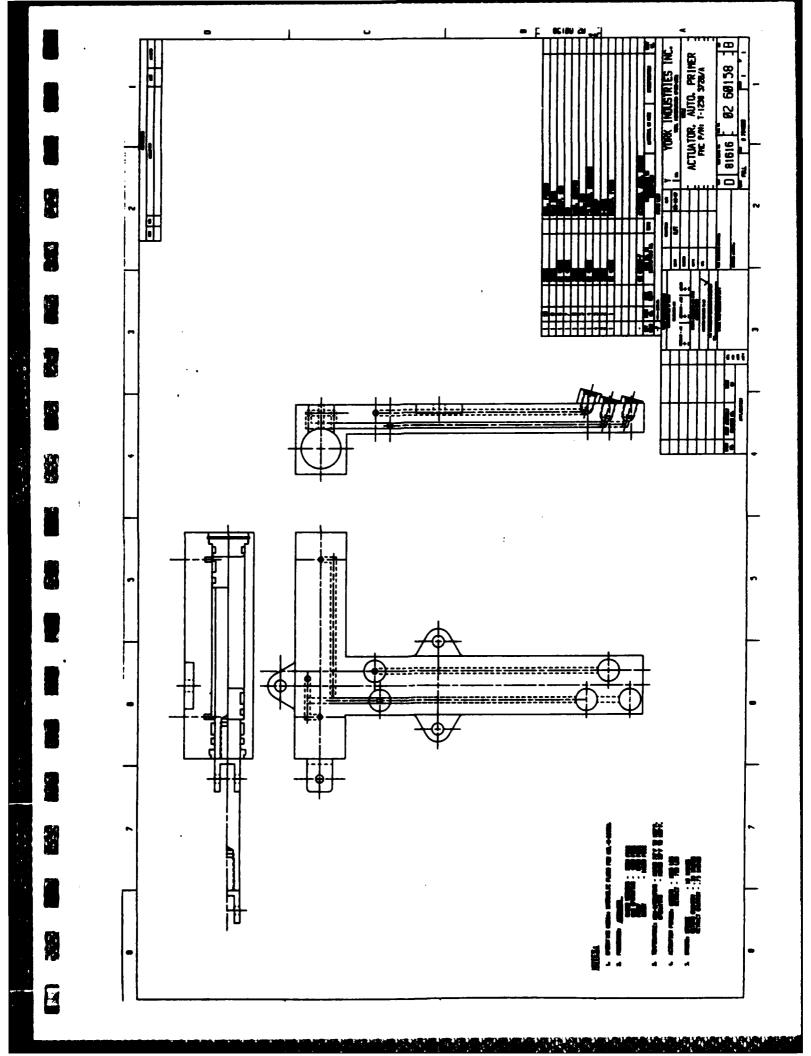
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DESCRIPTION: PRIMER ACTUATOR

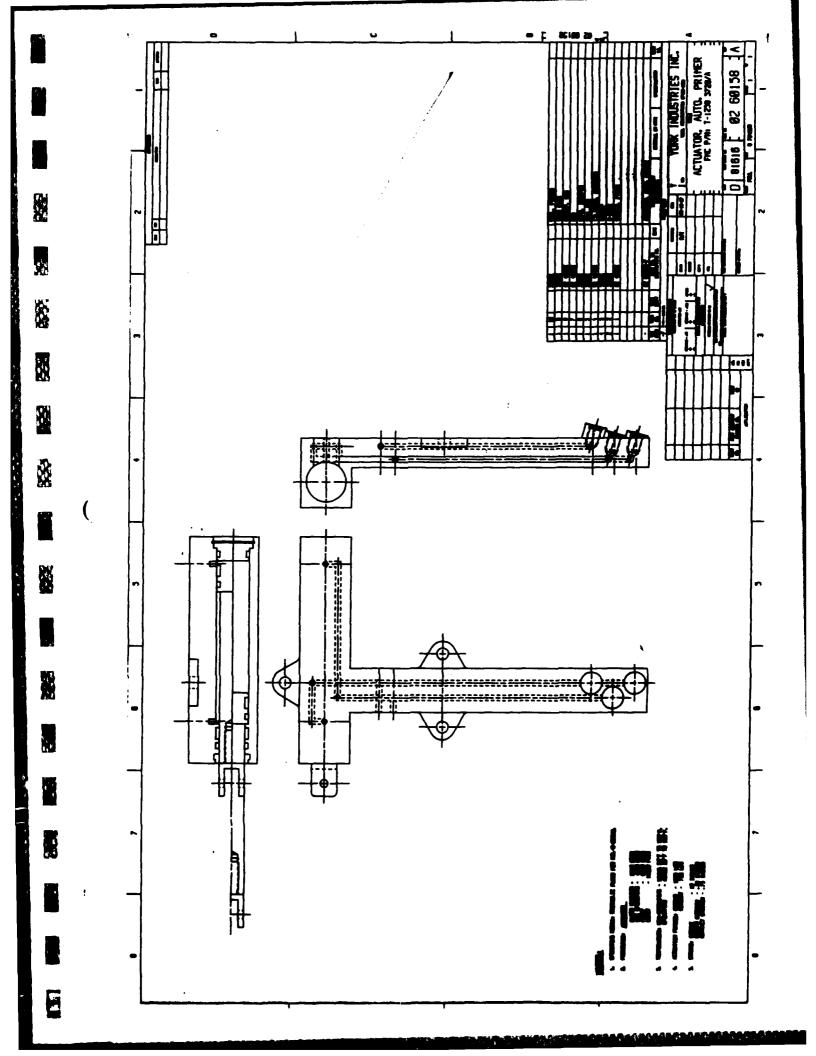
STATUS - PER YORK:

The concept drawing on this actuator was approximately 80% complete. Design provisions for extensive flexing of its mount and adjacent components were being evaluated. The weight of this unit exceeds its budget due to the extensive manifold incorporated into its requirements. Since there is little expectation of being able to reduce its weight to the budget level, it was recommended that its weight budget be approximately revised.



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DESCRIPTION: PRIMER ACTUATOR (Obsolete)



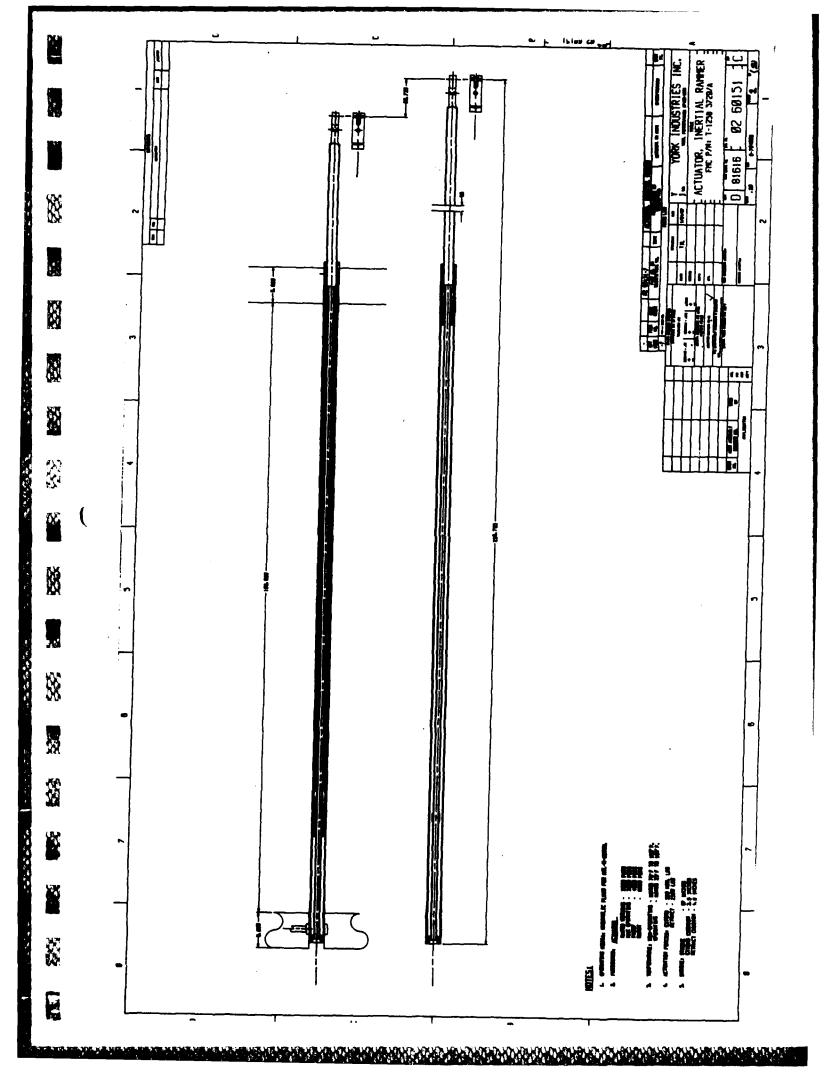
DESCRIPTION: RAPPER ACTUATOR

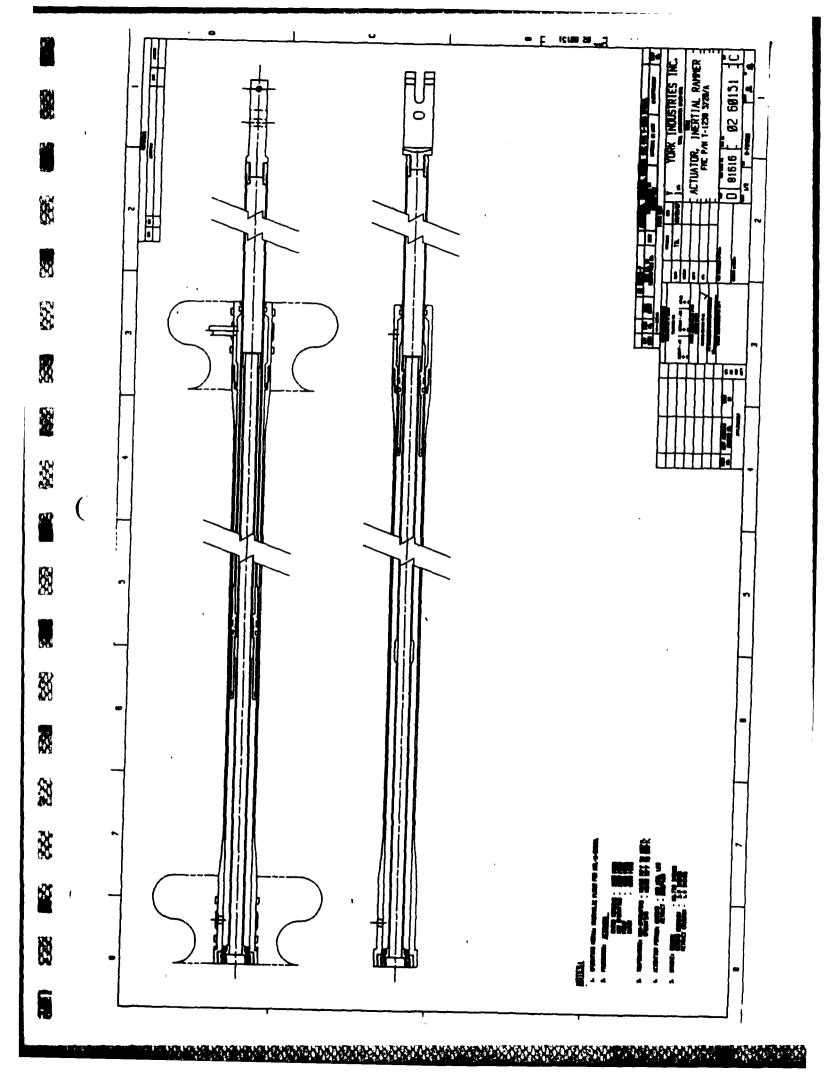
STATUS - PER YORK:

The concept drawing on this actuator was completed and the assembly drawing begun. An internal design review of fabricability and assembly potential problems was in progress. The design of this actuator permits extensive flexing in its mounts and possible problems were being evaluated. The weight of this unit exceeds its budget; therefore, further weight reduction effort is anticipated.

STATUS - PER FMC:

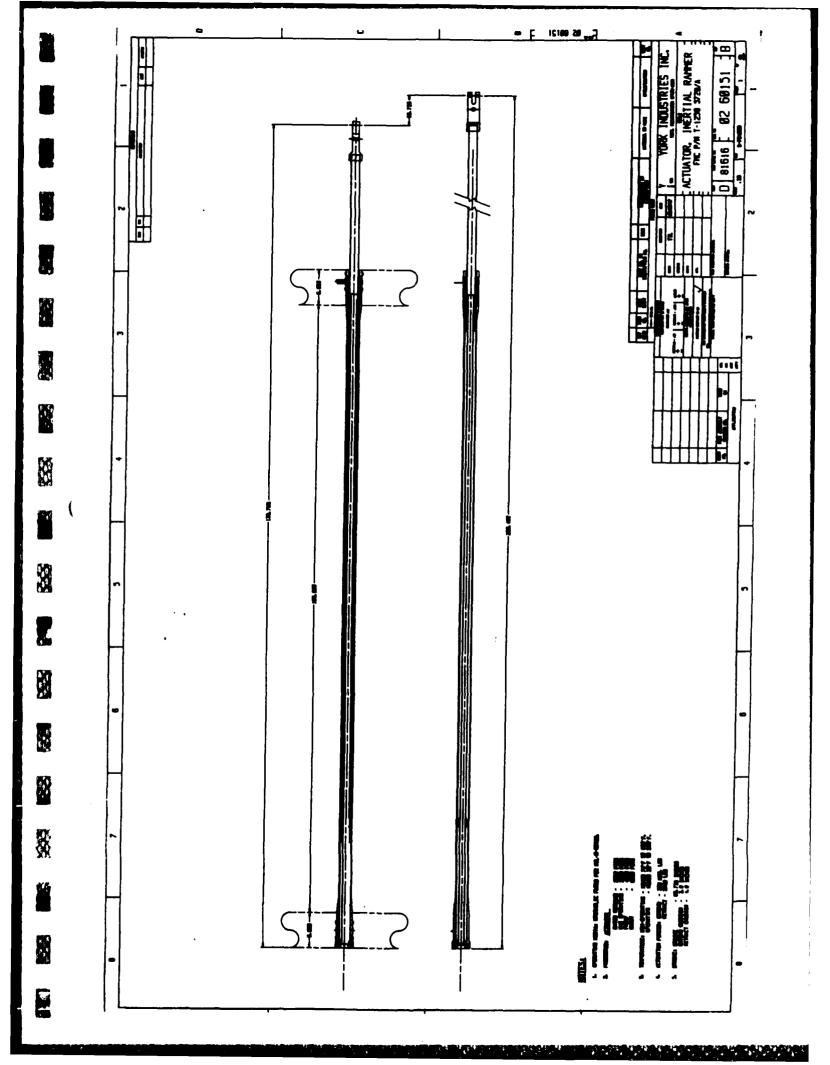
Rod size was determined by 18-20 g LAPES - load (calculations by Jeff Ireland).

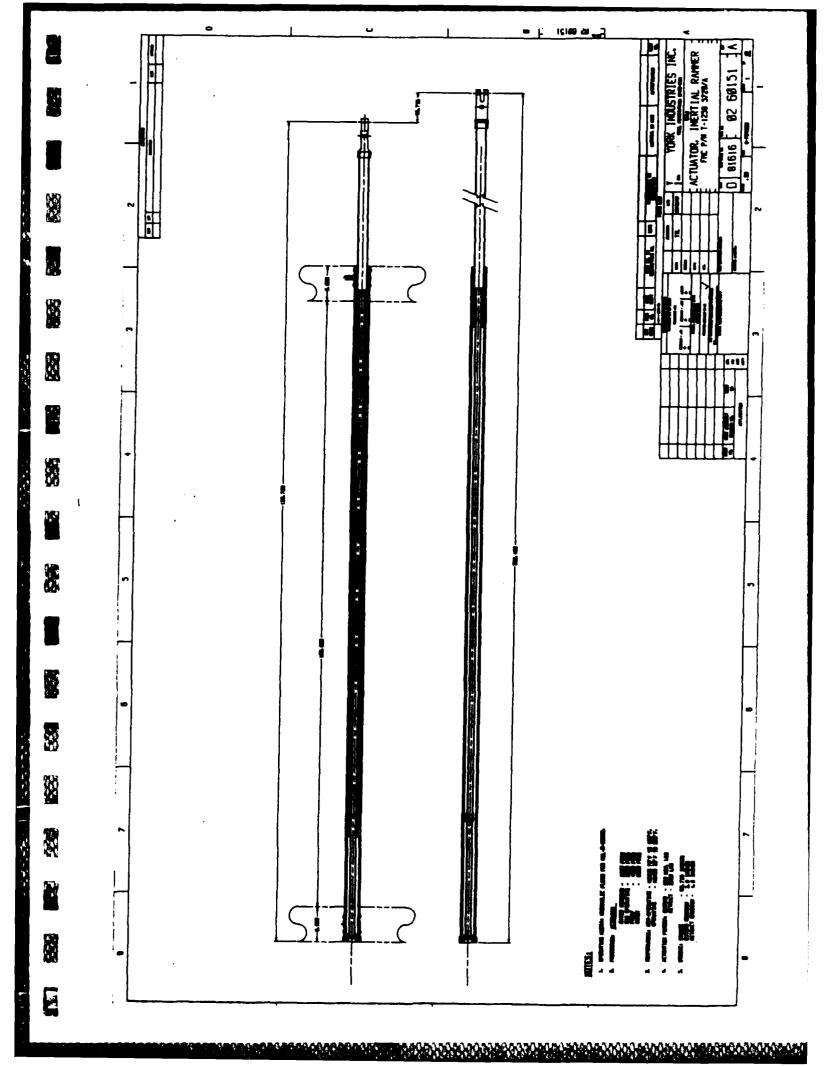


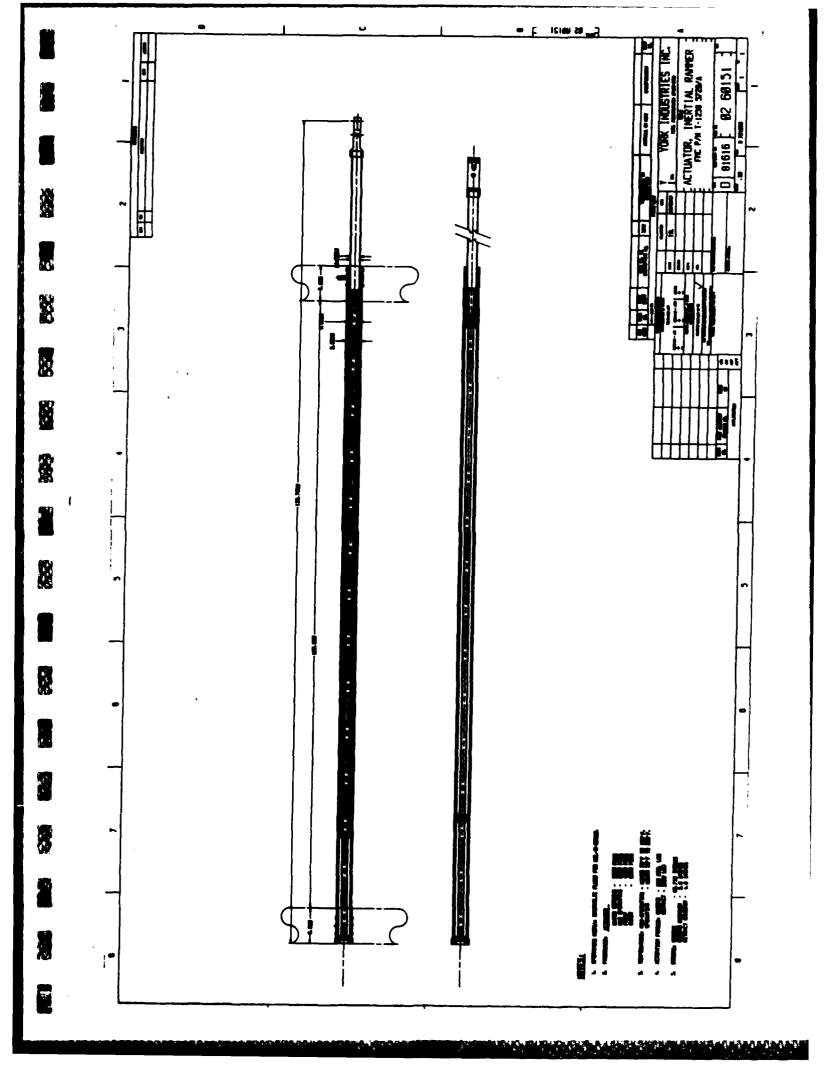


DESCRIPTION: RAMMER ACTUATOR (Obsolete)

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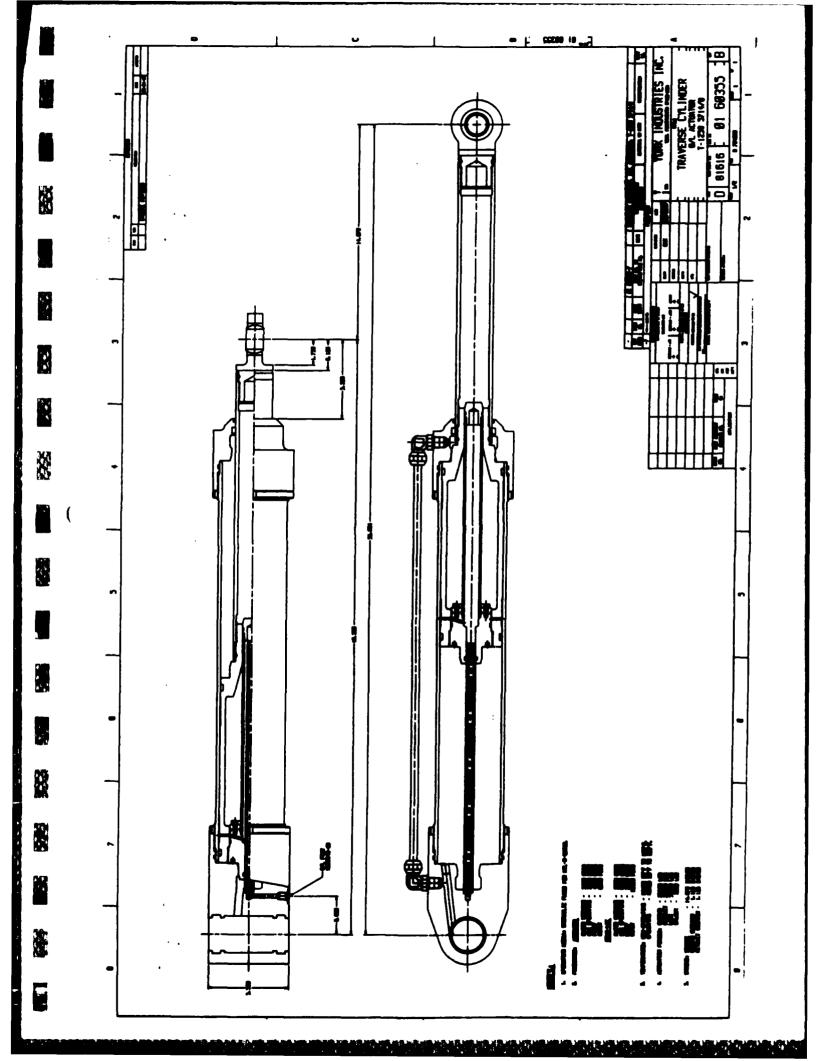


DESCRIPTION: TRAVERSE ACTUATOR

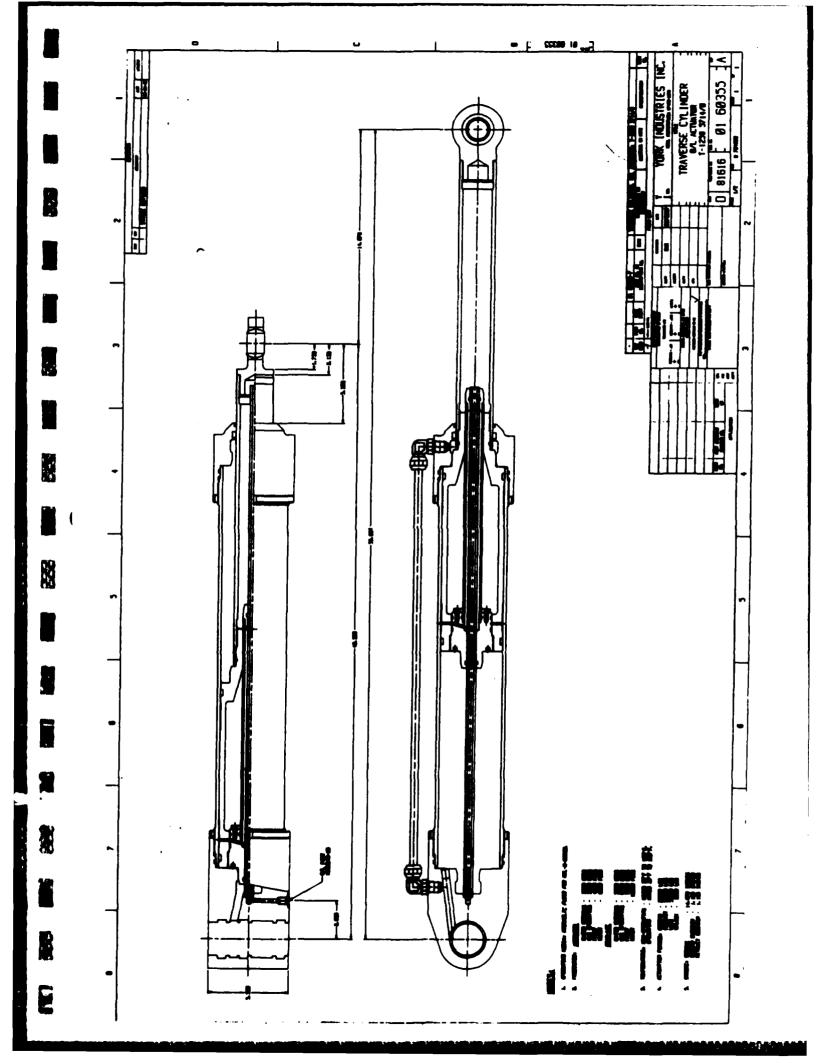
STATUS - PER YORK:

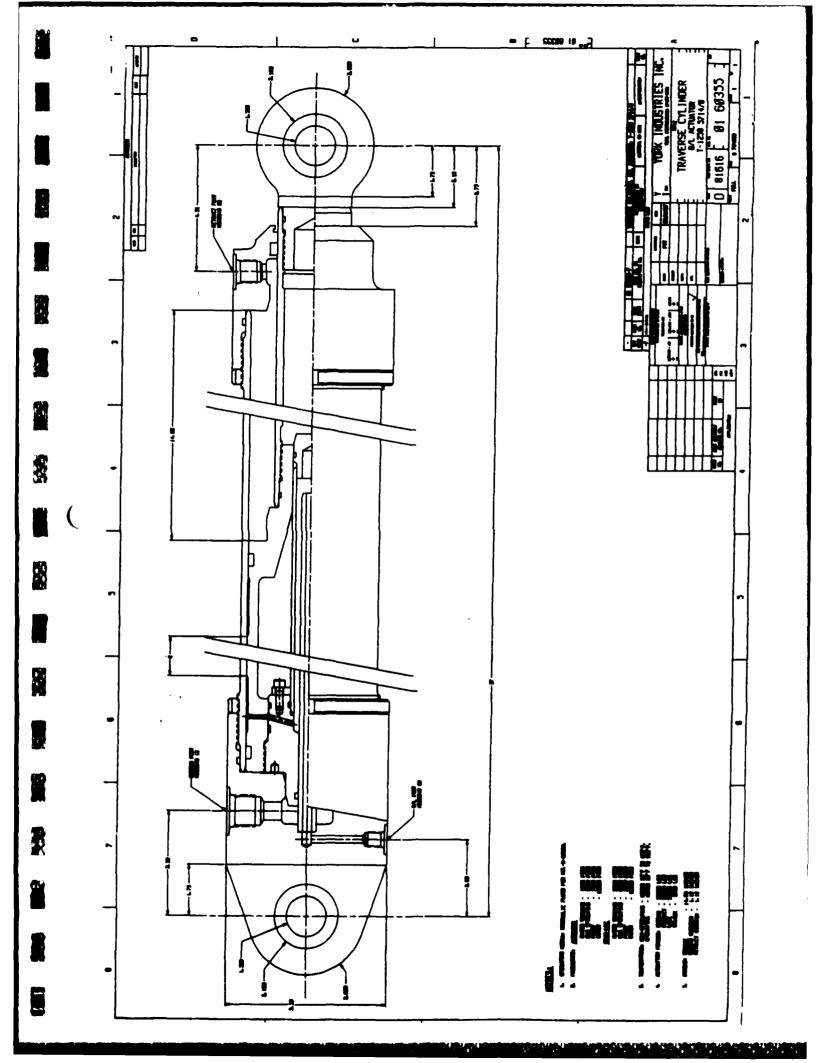
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The concept drawing is complete, but the stroke must be changed to the requirements of the March 6 coordination meeting. The projected weight estimate is over the allotted target weight due to the increase in stroke, thus another weight reduction pass would have been required.



DESCRIPTION: TRAVERSE ACTUATOR (Obsolete)





DESCRIPTION: WALKING BEAM ACTUATOR - LH FRONT

STATUS - PER YORK:

The concept drawing on this component had been completed and the assembly drawing was being revised to incorporate 2 inches of free travel in the transit mode. Several approaches to obtain free travel were being evaluated which would have been added to the assembly drawing when complete. The design provisions for free travel were being evaluated on the rear actuators and would have been added to these actuators when complete.

An extended stroke pin lock was incorporated into the actuator. This lock is actuated by hydraulic pressure and provides a flag of lock/unlock status.

The assembly drawing was being revised to mount the FMC specified control valve directly on the actuator.

This unit, as revised, exceeds its weight budget by 20% and required further design effort directed at weight reduction.

STATUS - PER PMC:

See C/270 (Dynamic Analysis of Walking Beam Actuators) for description of options under evaluation to solve road-input-induced fluid flow problem.

Mote also the 3500 PSI safety fuze (item 21), to further protect LTHD hardware against potential damage due to unanticipated road-input bump velocities beyond design limits, pending acquisition of actual road-inputs data.

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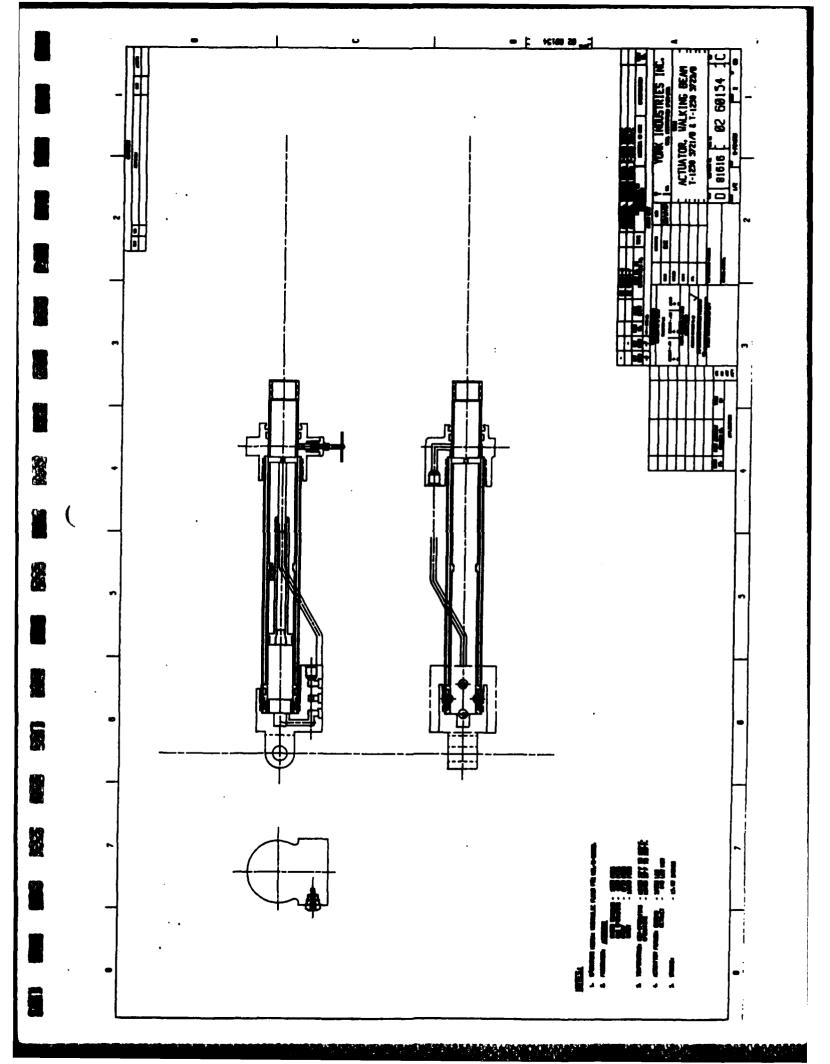
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DESCRIPTION: WALKING BEAM ACTUATOR - LH FRONT (Obsolete)

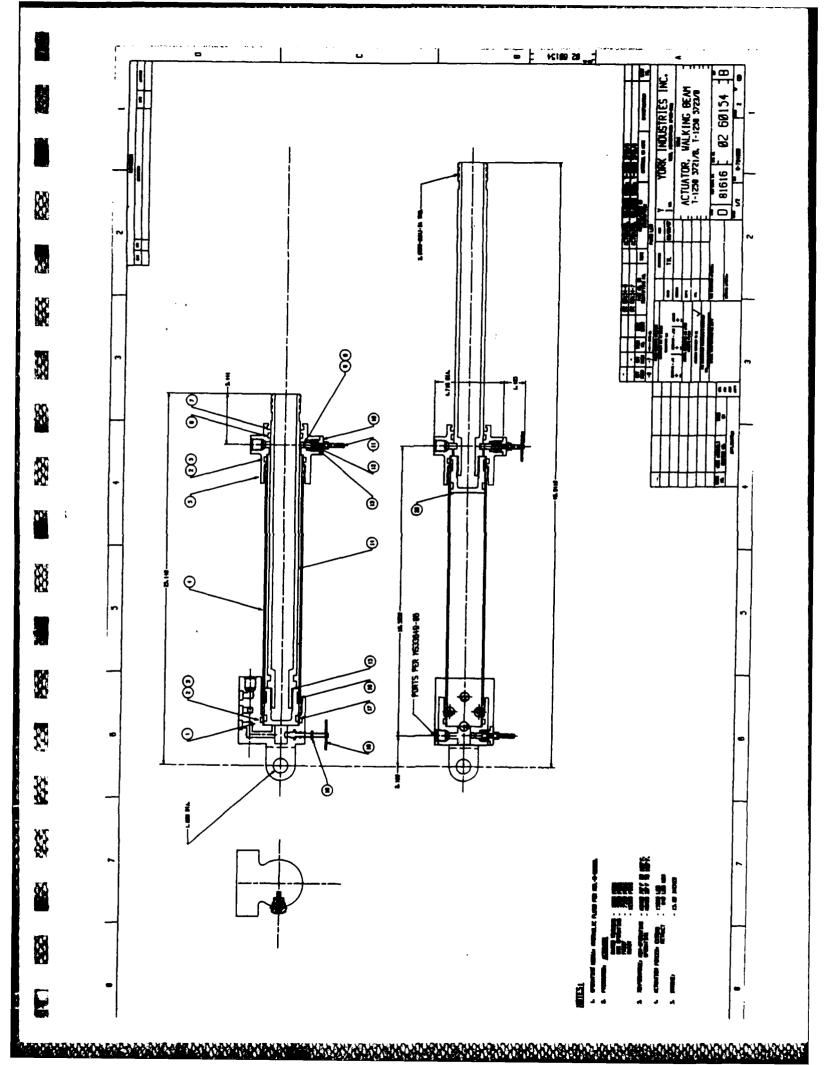
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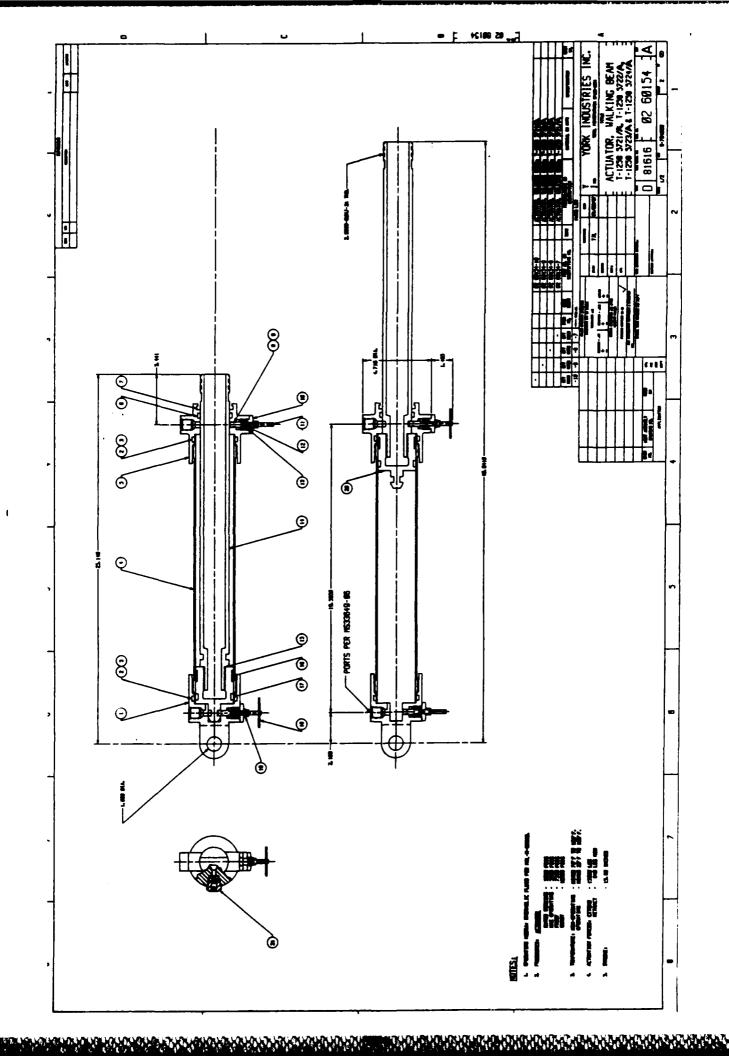
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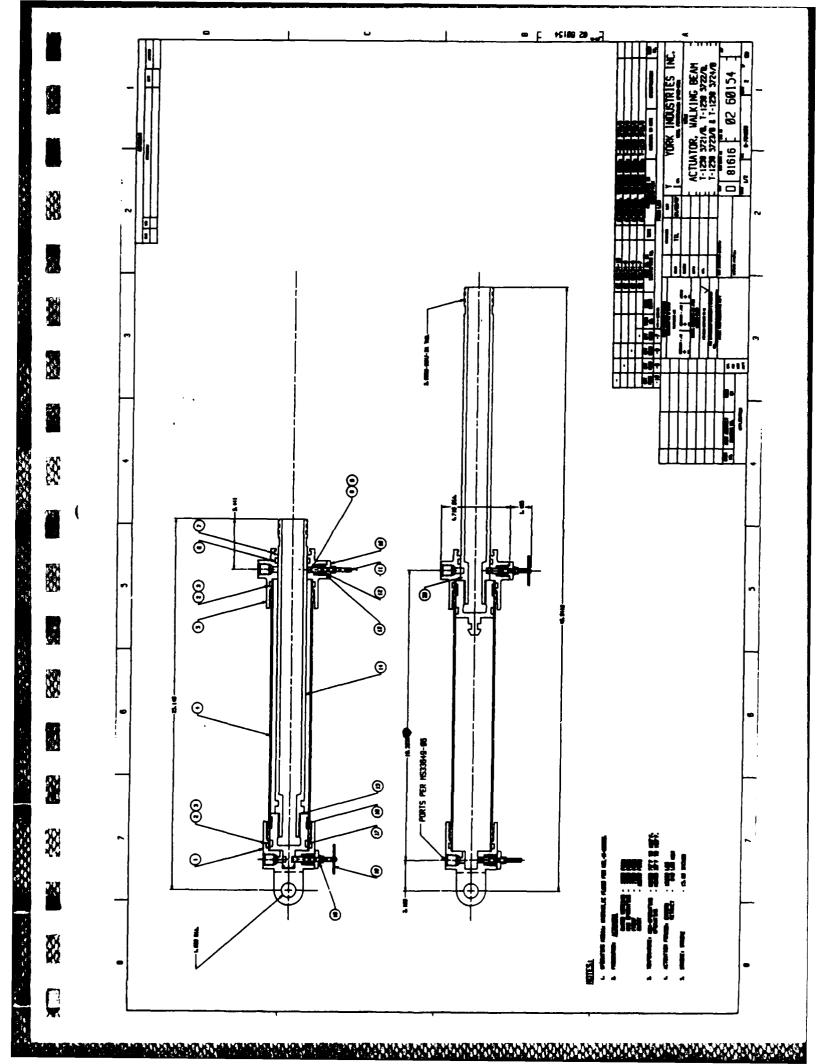
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DESCRIPTION: WALKING BRAM ACTUATOR - LH REAR

STATUS - PER YORK:

The concept drawing on this component had been completed and the assembly drawing was being revised to incorporate 2 inches of free travel in the transit mode. Several approaches to obtain free travel were being evaluated which would have been added to the assembly drawing when complete.

The extended stroke pin lock was also incorporated into the actuator.

The assembly drawing was being revised to mount the FMC specified control valve directly on the actuator.

This unit, as revised, exceeds its weight budget by 20% and required further design effort directed at weight reduction.

STATUS - PER FMC:

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See E/260

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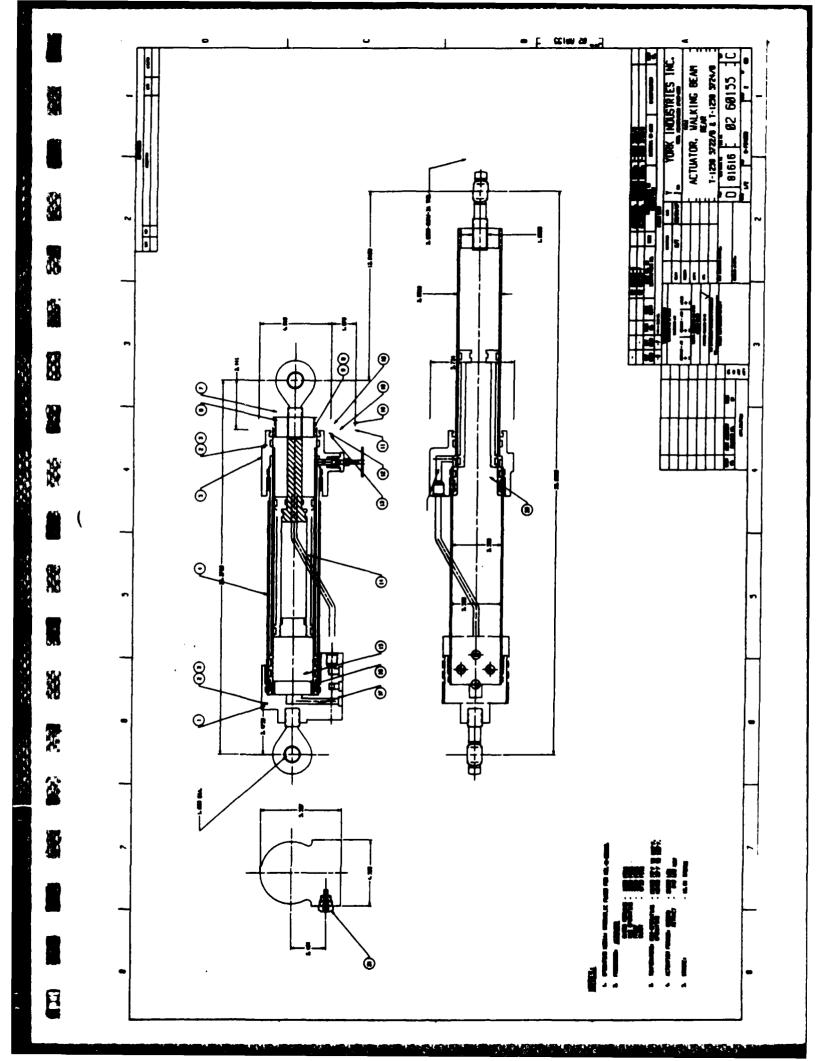
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DESCRIPTION: WALKING BEAM ACTUATOR - RH FRONT

STATUS - See E/260

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DESCRIPTION: WALKING BRAM ACTUATOR - RH REAR

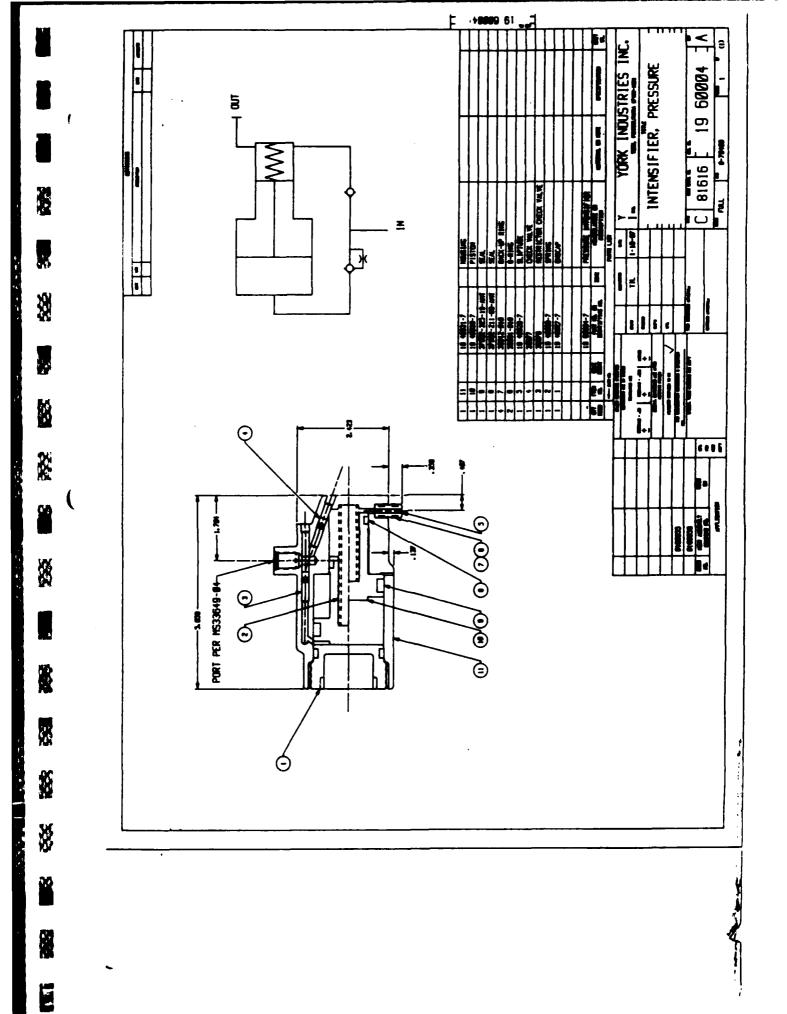
STATUS - See E/270

DESCRIPTION: BEAR-LOC INTENSIFIER ASSEMBLY

FMC COMMENT:

Operation of the Bear-Loc at an intensified pressure facilitates a smaller and lighter Bear-Loc for the same holding force. Since the intensifier is mounted on the actuator it serves, and hardlined by York, it's presence is somewhat transparent to the hydraulic system.

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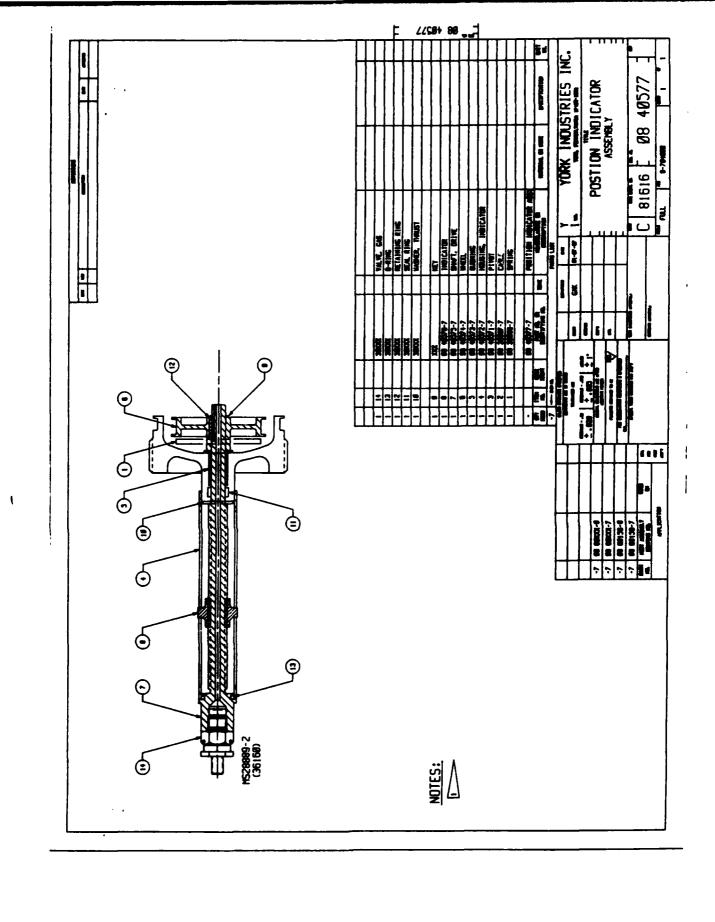
DESCRIPTION: ACCUMULATOR VOLUME (PISTON POSITION) INDICATOR ASSEMBLY

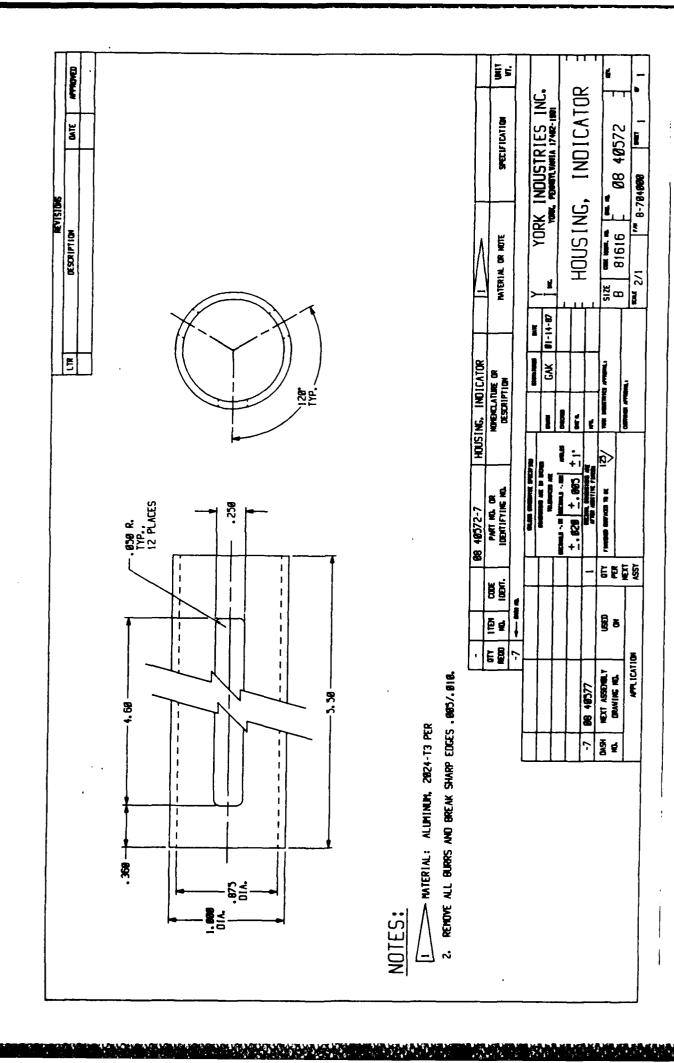
FMC COMMENT:

This method for indicating accumulater oil volume was chosen over the traditional indicator rod for weight and space reasons.

One end of a cable is attached to the piston while the other end is Vaceled. The reel is (torsionally) spring-loaded. A stud is attached to reel and turns with it. A nut is threaded onto the stud, but not allowed to rotate with the stud. Thus, piston movement turns the reel, which rotates the stud, and displaces the nut. The nut travel is about 4" and thus serves as a volume indicator.

An indicator similar to this has been flight certified and is in use on one of the F-IX fighter aircraft (I can't remember which one).





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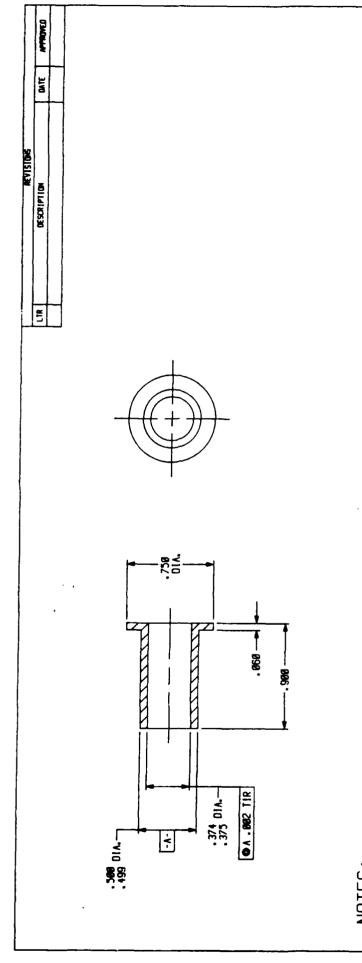
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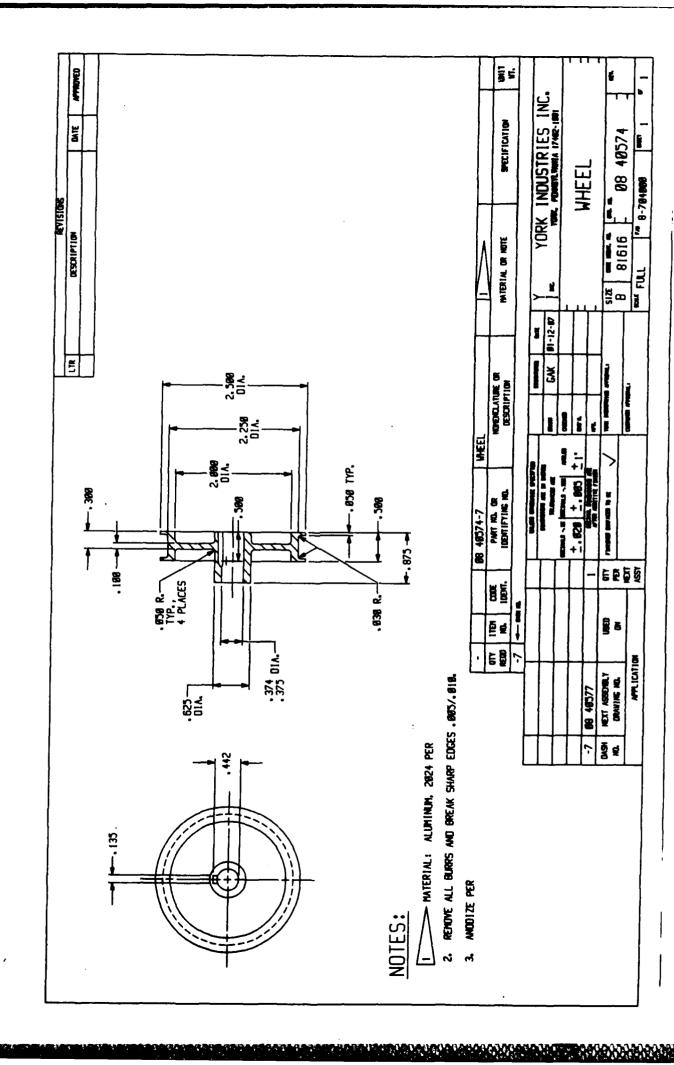
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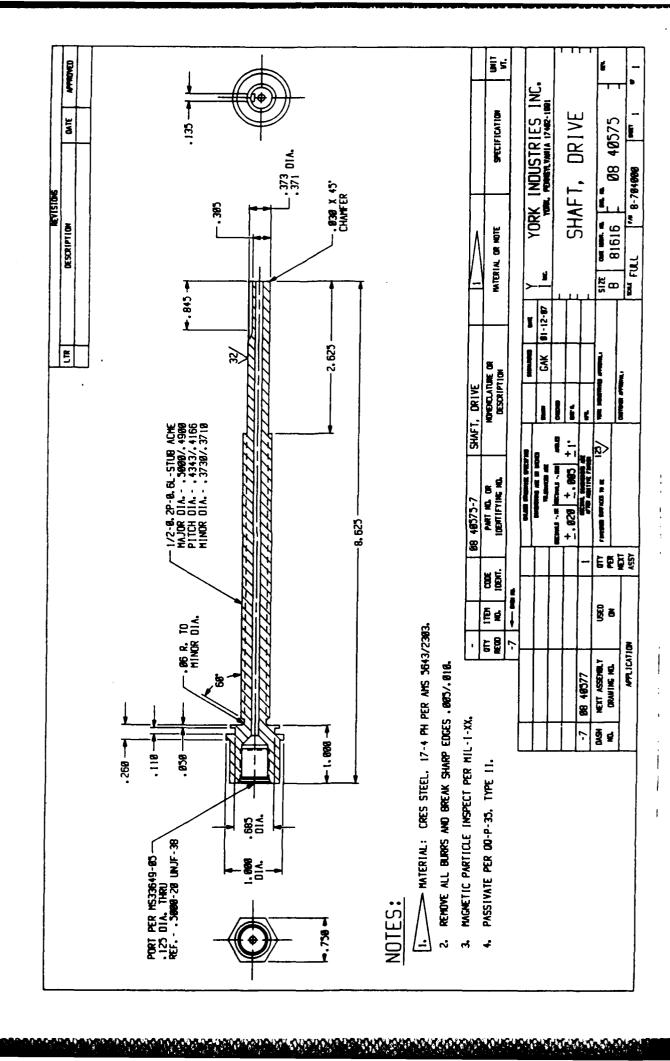
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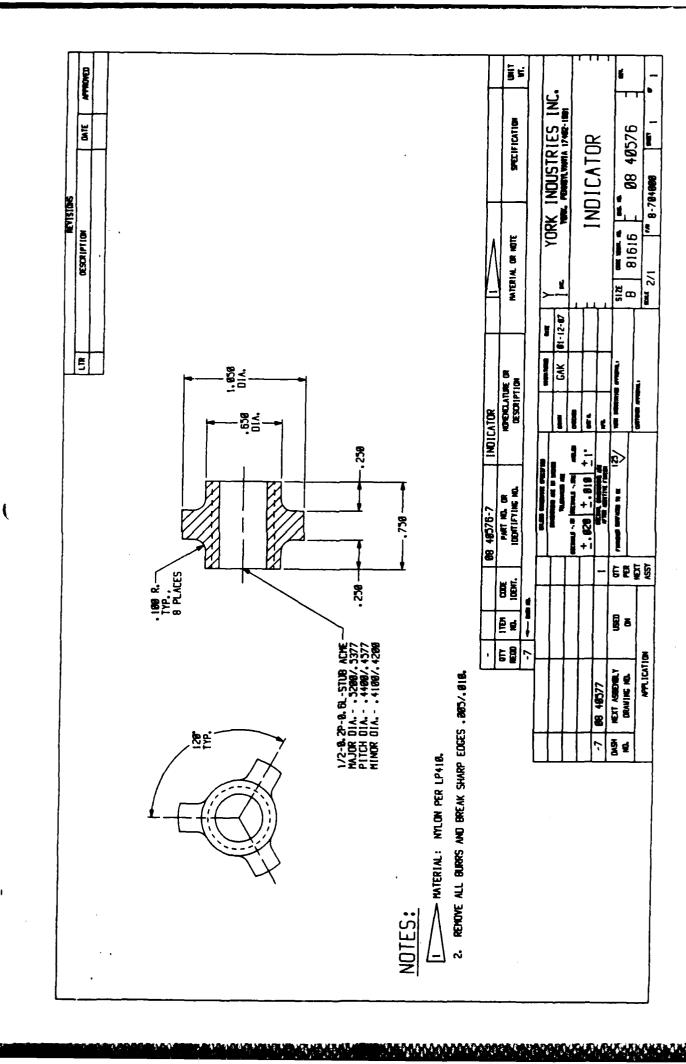
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